



Università dell'Aquila

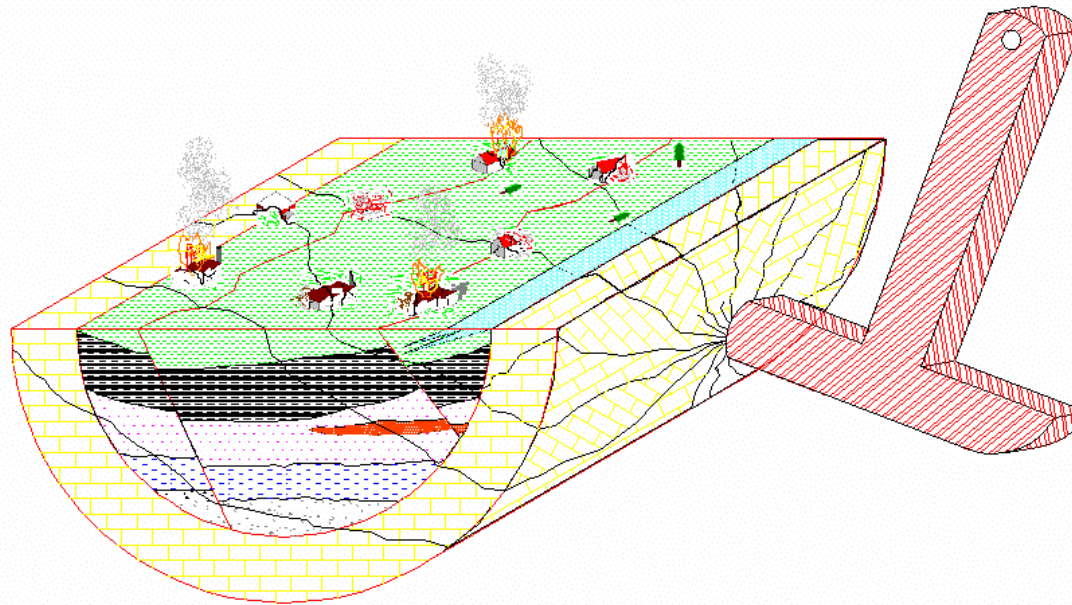
Gruppo Geotecnico Dipartimento DISAT

Calabrese, Marchetti, Monaco, Totani

MISURE DI V_s (Go) mediante DILATOMETRO SISMICO

Prof. Silvano Marchetti

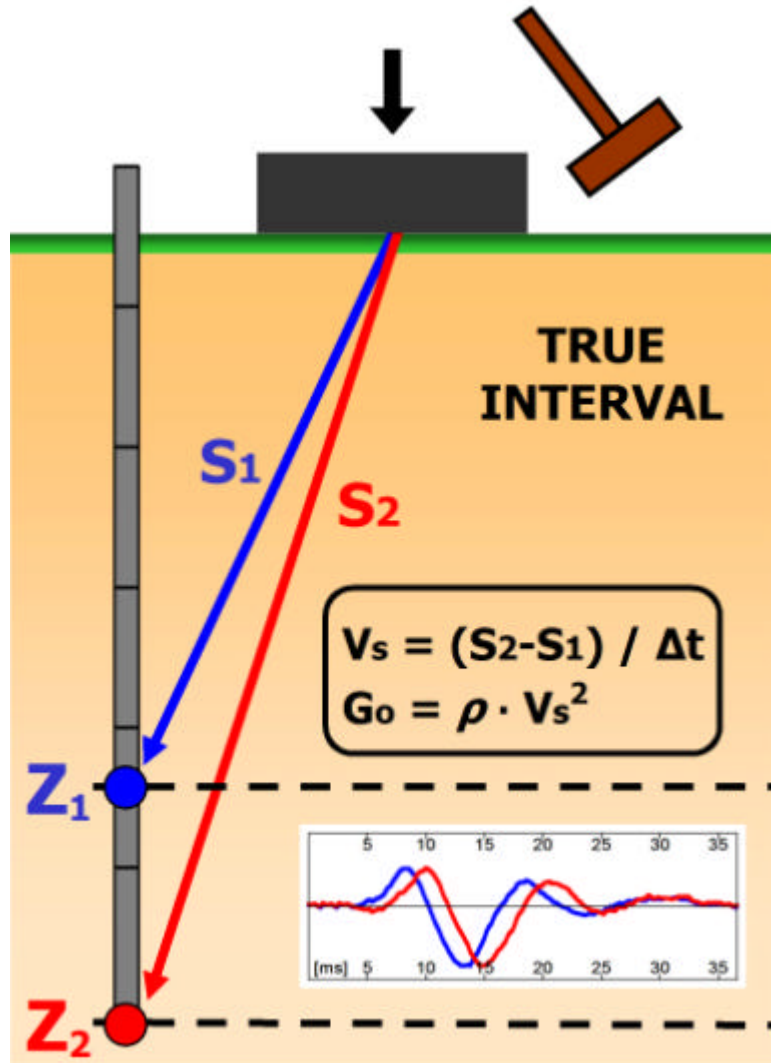
Risposta sismica locale



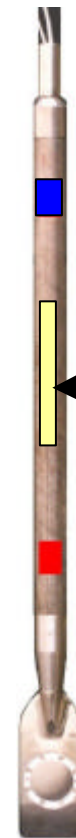
- V_s (G_0): mattoni basilari risposta sismica
- Condividere esperienza SDMT dal 1999

Mayne (1999) "Small- and Large-Strain Soil Properties from Seismic Flat Dilatometer Tests", Proc. Pre-failure Deformation Characteristics of Geomaterials, Jamiolkowski et al. editors, Torino.

DILATOMETRO SISMICO



SDMT Combinazione S - DMT



2 ricevitori

No primo arrivo...

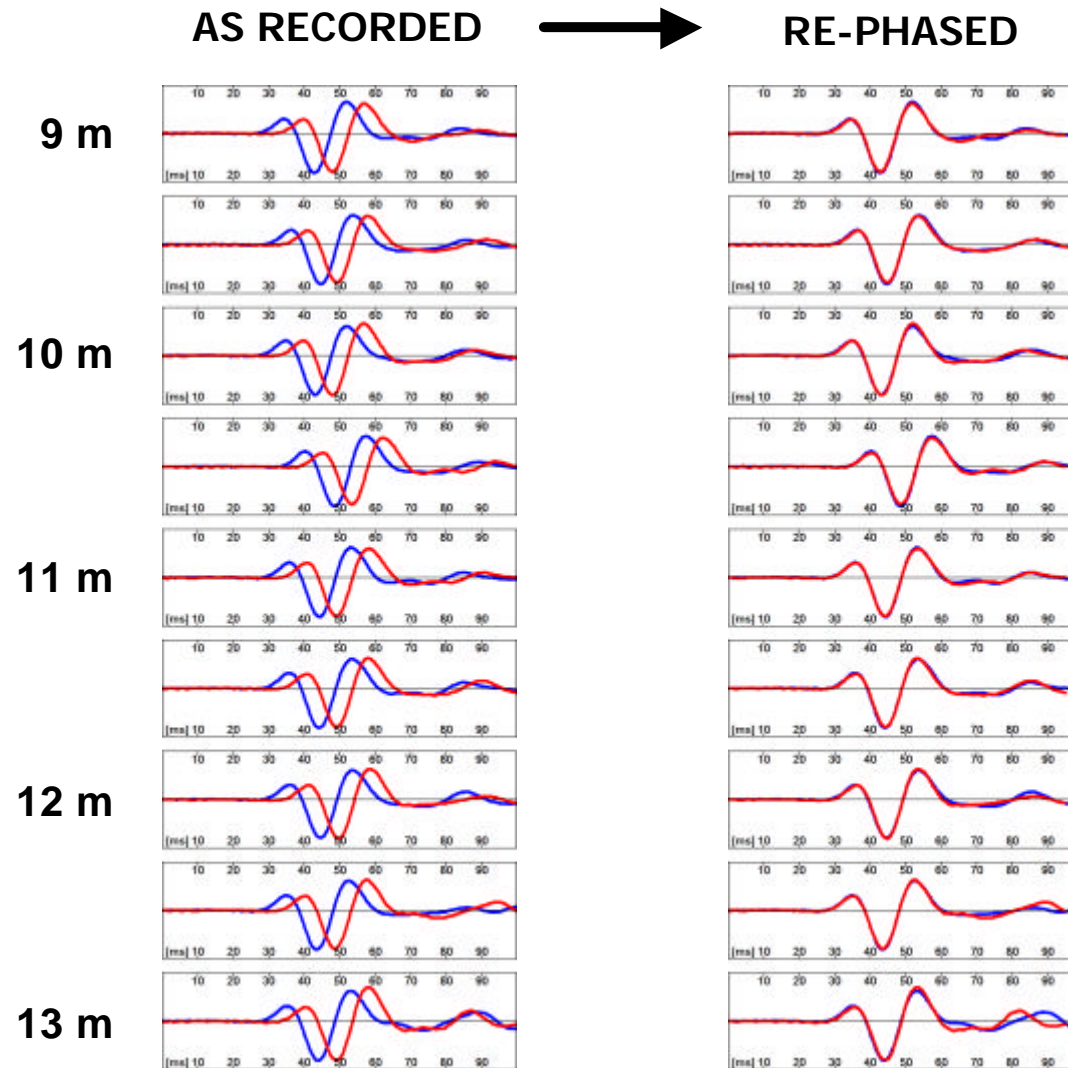
Stesso impulso

← **Amplificato + digitalizzato
in profondità**

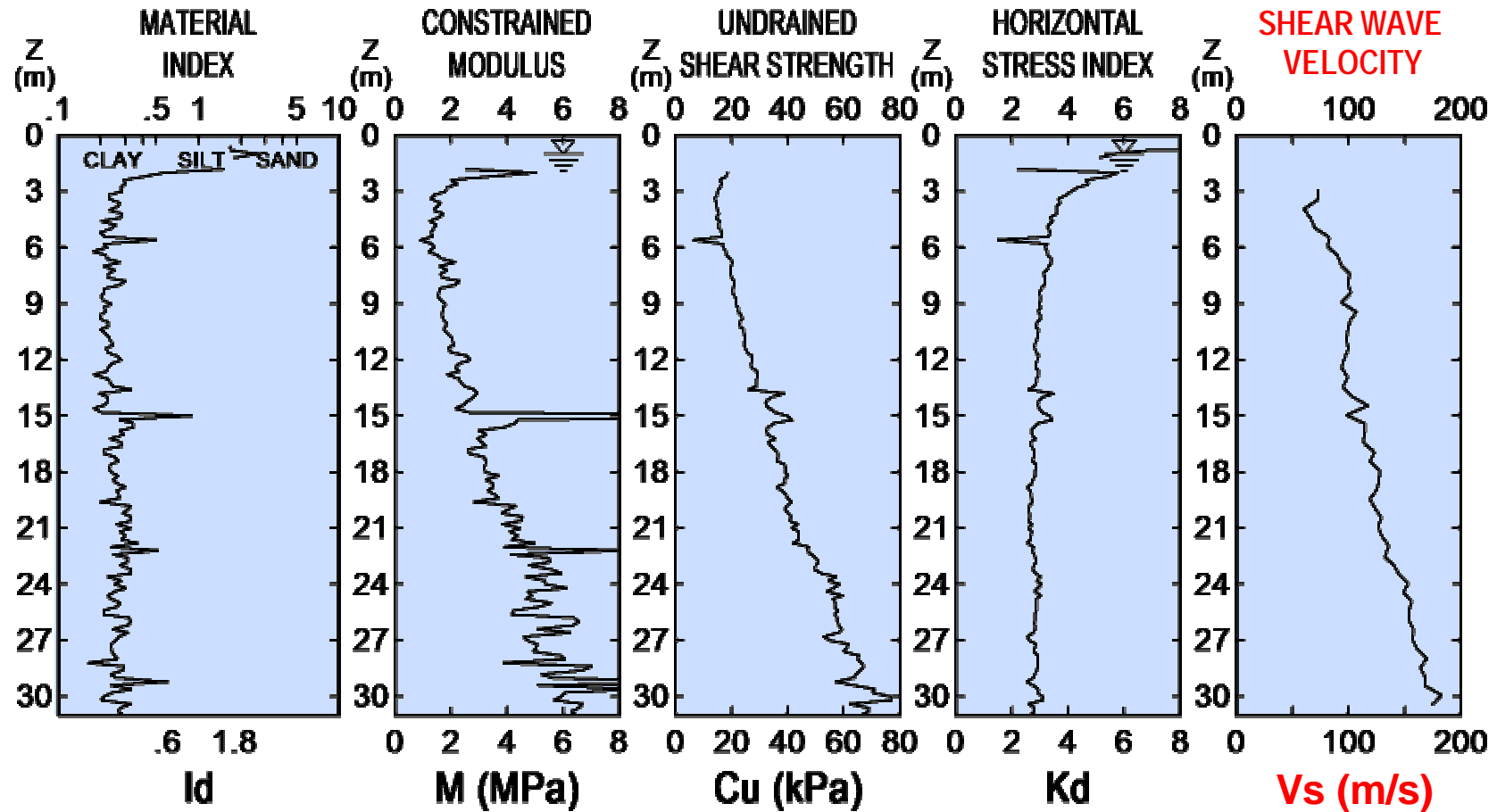
**No foro – aderenza – indep.
operatore (e interpret.)**

Rapida & economica

SDMT at Fucino (June 2004)



SDMT RESULTS – Fucino



Repeatability of Vs

Fucino

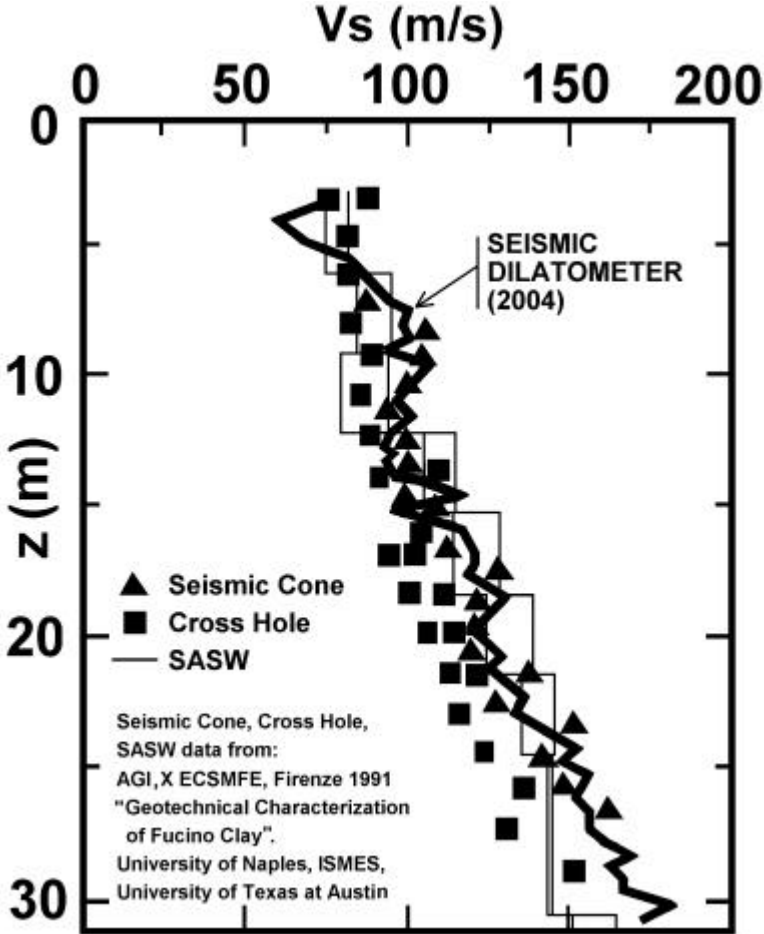
Each Vs corresponds to a blow of the hammer

Differences of Vs: 1 m/s

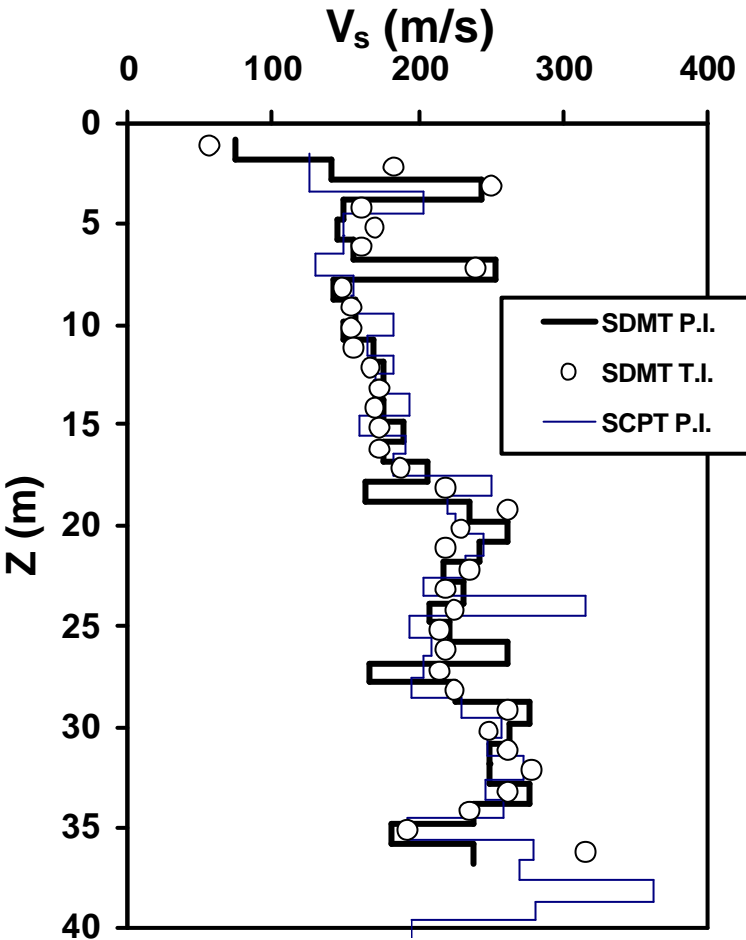
| Z [m] | Vs [m/s] | | |
|-------|----------|-----|-----|
| 10.0 | 101 | 101 | |
| 10.5 | 99 | 99 | |
| 11.0 | 98 | 98 | |
| 11.5 | 99 | 100 | |
| 12.0 | 97 | 96 | |
| 12.5 | 94 | 94 | |
| 13.0 | 99 | 99 | |
| 13.5 | 95 | 95 | |
| 14.0 | 103 | 103 | |
| 14.5 | 117 | 117 | 117 |
| 15.0 | 98 | 98 | 98 |
| 15.5 | 115 | 115 | |
| 16.0 | 114 | 114 | |
| 16.5 | 113 | 113 | |
| 17.0 | 122 | 123 | |
| 17.5 | 119 | 119 | |
| 18.0 | 128 | 128 | |
| 18.5 | 127 | 127 | |
| 19.0 | 125 | 125 | |
| 19.5 | 119 | 119 | |
| 20.0 | 124 | 124 | 124 |

Comparisons Vs-SDMT

Fucino Research Site



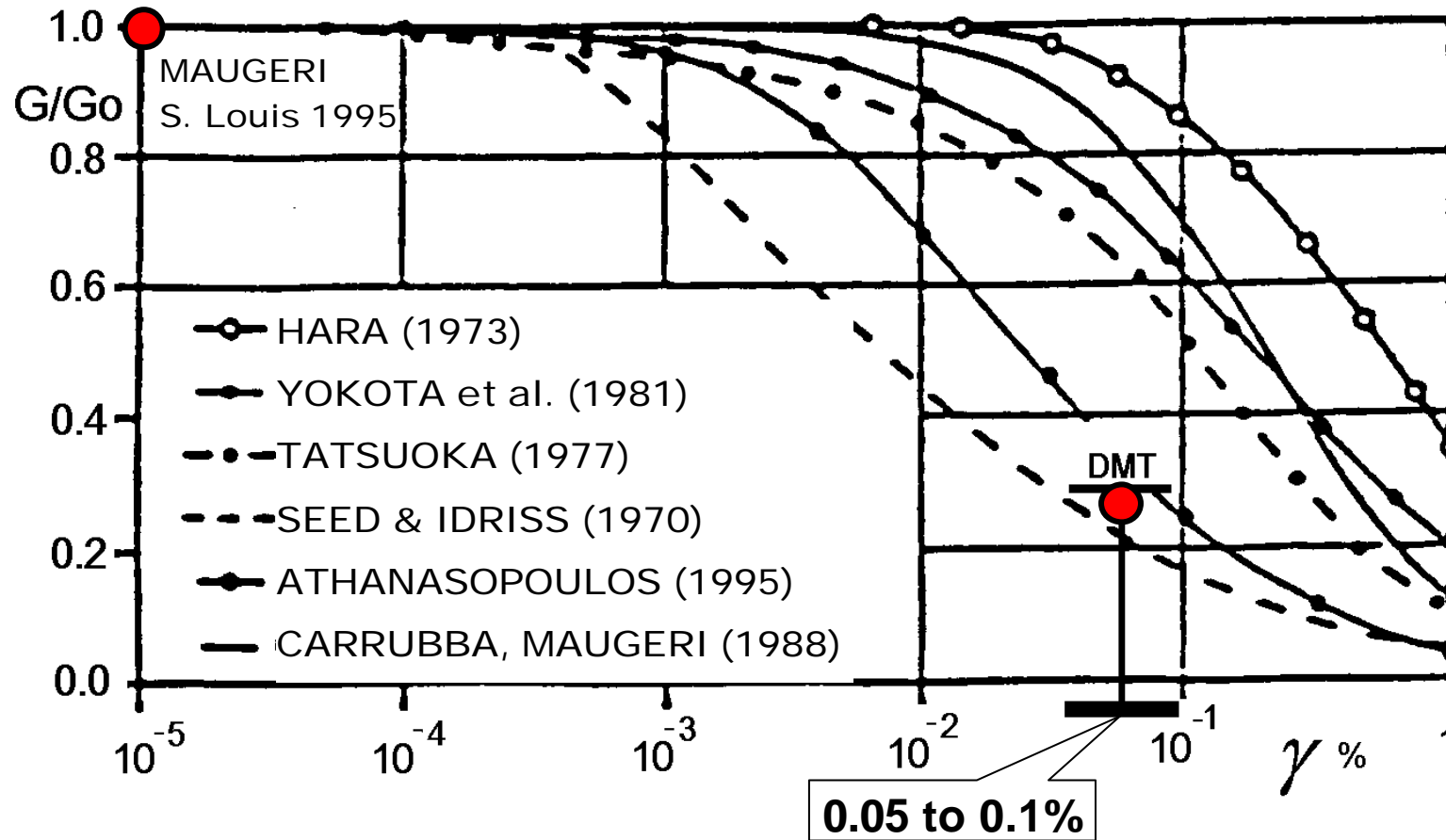
Venezia - Treporti



Hammer



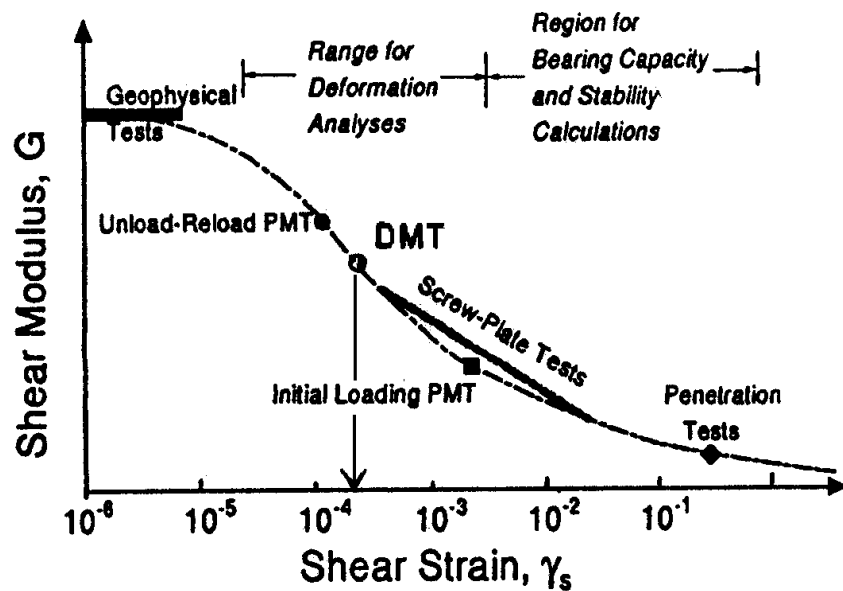
SDMT misura, oltre G_0 , un modulo a "deformazioni operative" (cedimenti statici fondazioni)



Due punti aiutano a scegliere la curva $G - g$

γ - Range for DMT Modulus

Mayne – Insitu 2001, Bali



Ishihara – Insitu 2001, Bali

| | Small strain | Medium strain | Large strain |
|-----------------|--|--|--|
| | ← No dilatancy → | | ← Dilatancy → |
| Level of strain | 10^5 | 10^{-4} | 10^{-3} 10^{-2} 10^1 |
| In-situ tests | <ul style="list-style-type: none"> • Down hole • Cross hole • SASW | <ul style="list-style-type: none"> • Presso-meter • Plate loading • Dilatometer | <ul style="list-style-type: none"> • SPT • CPT • Vane |
| Lab. tests | <ul style="list-style-type: none"> • Resonant column • Wave propagation • Bender element • LDT | <ul style="list-style-type: none"> • Tests on undisturbed samples | |

DMT FOR LIQUEFACTION

- Factors (SH) making DMT + sensitive to compaction and + accurate settlements :are known to affect "liquefiability"

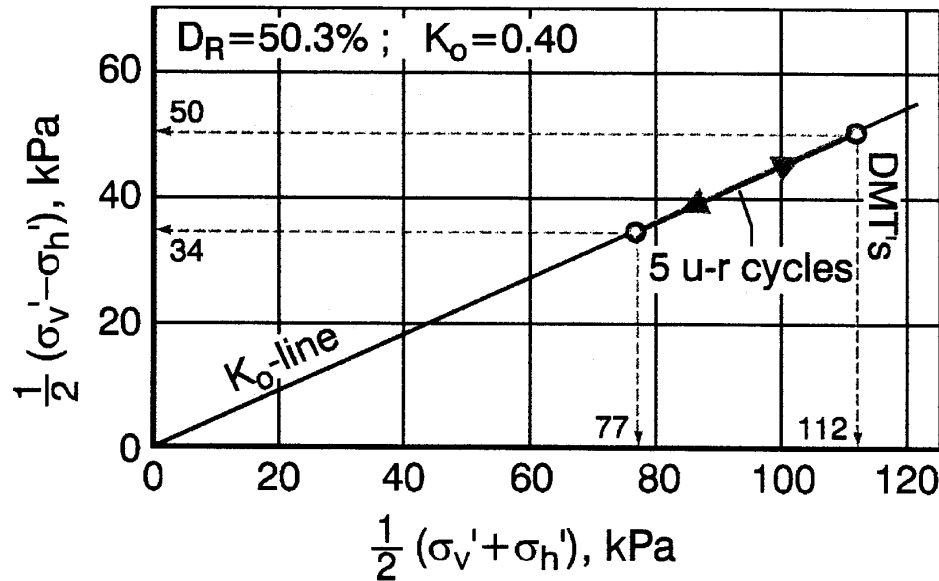
Jamiolkowski's res. group (S.F. 1985): "*reliable predictions [of liquefiability] in complex stress-history deposits require the development of some new in situ device [other than CPT or SPT] more sensitive to the effects of past stress and strain histories".*

- Less disruptive insertion in loose sand

Clean sand is safe against Liquefaction (M=7.5 earthquakes) if $K_d > :$

| Seismicity of the area | a_{max}/g | K_d, min |
|------------------------|-------------|------------|
| Nonseismic | / | 1.7 |
| Low seismicity | 0.15 | 4.2 |
| Average seismicity | 0.25 | 5.0 |
| High seismicity | 0.35 | 5.5 |

SENSITIVITY of PENETRATION RESISTANCE and K_D -DMT to PRESTRAIN



Calibration
Chamber

Jamiolkowski
Res. group

| | I_D (-) | K_D (-) | E_D (MPa) | M_D (MPa) | q_D (MPa) |
|--------|--------------|--------------|----------------|----------------|----------------|
| Before | 2.62 | 1.98 | 29.0 | 30.3 | 16.0 |
| After | 2.41 | 2.38 | 31.8 | 37.8 | 16.4 |

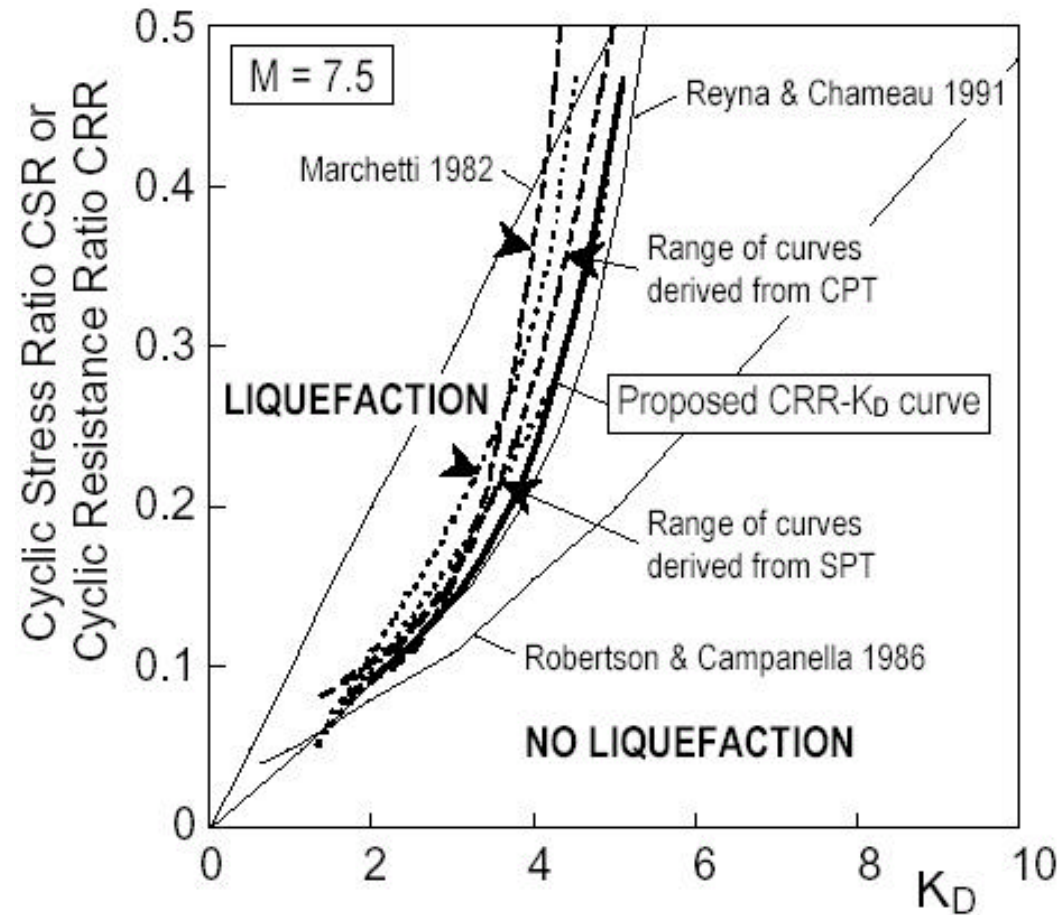
+20%

+3%

Kd increase

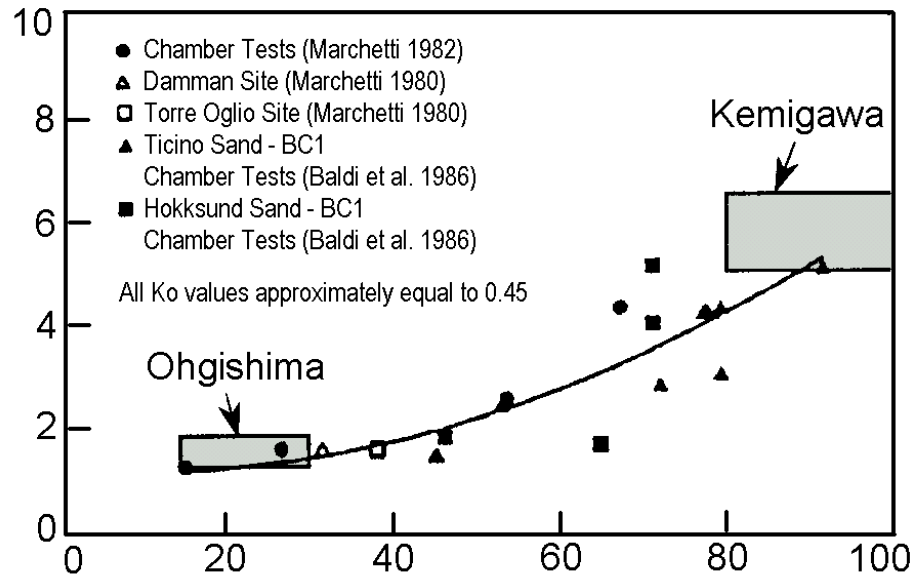
Penetr. resist.
increase

Curve CRR-K_d per stimare liquefacibilità mediante DMT con procedura di Seed-Idris

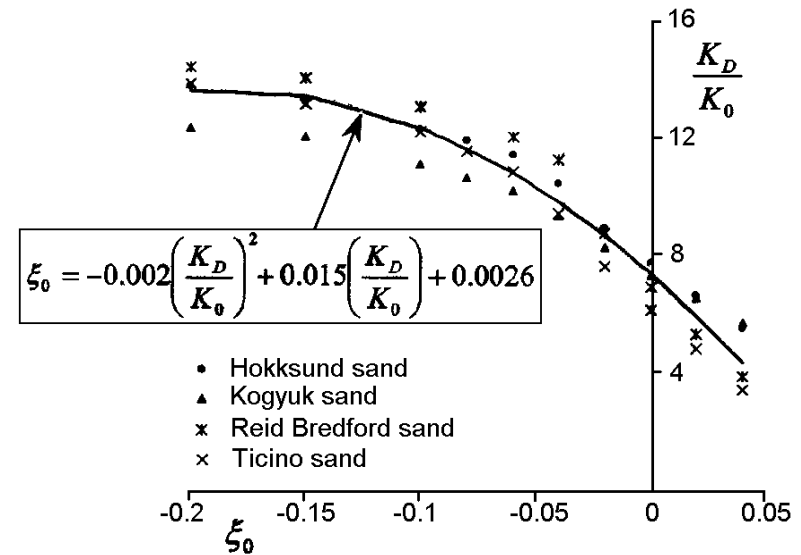


Monaco et al., Osaka 2005

Correlations K_D - D_r and K_D - ξ



Correlation K_D - D_r for NC uncemented sands (Reyna & Chameau 1991), also including Ohgishima and Kemigawa datapoints obtained by Tanaka & Tanaka (1998) on high quality frozen samples

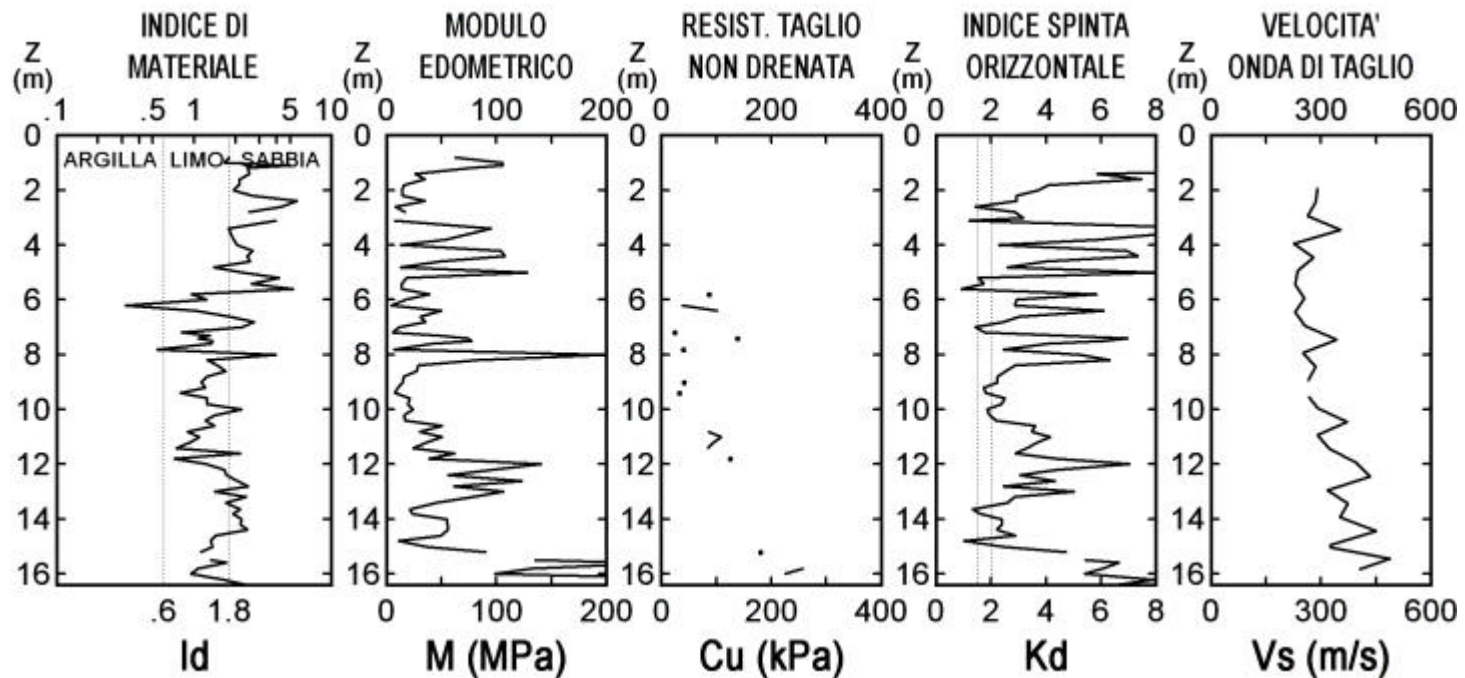


Average correlation K_D - in situ state parameter ξ_0 (Yu 2004)



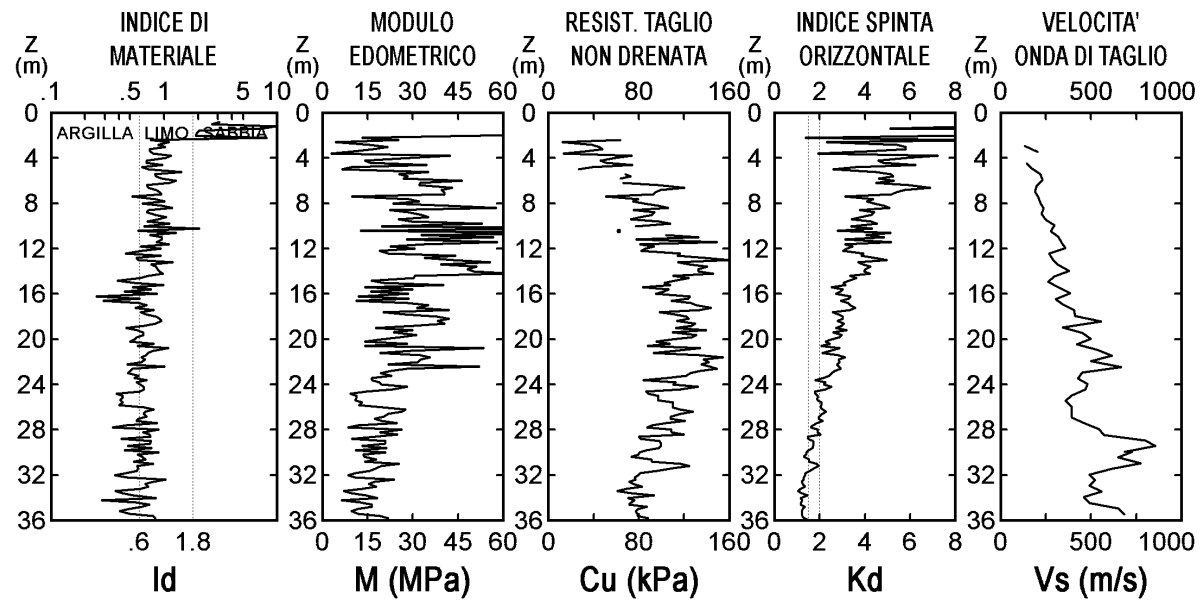
SDMT Studio Pilota Benevento

GNDT - Proff.
Vinale e Simonelli



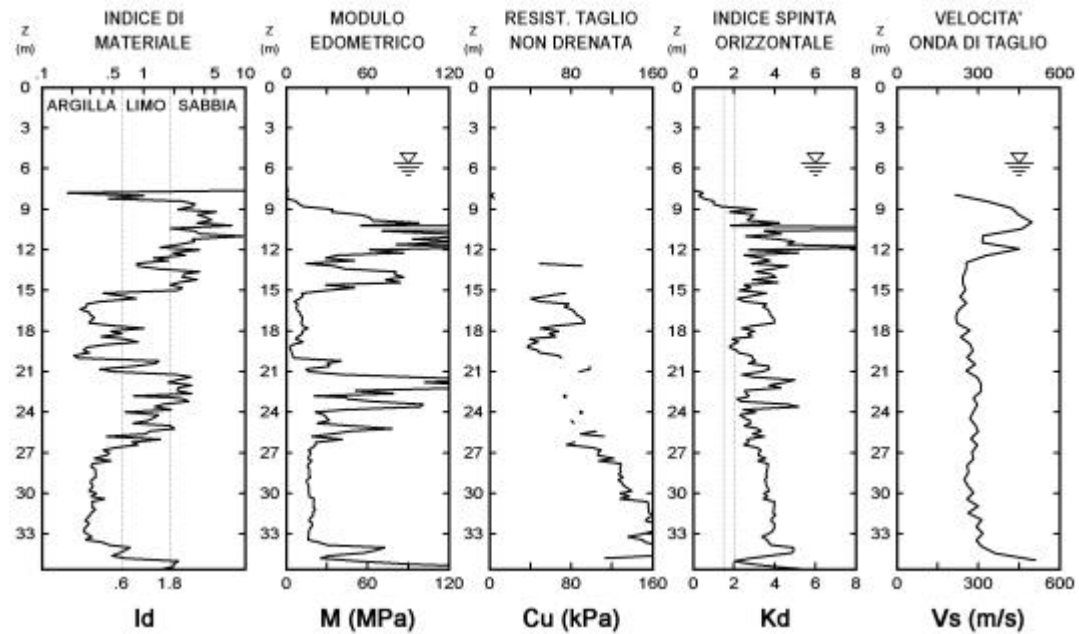


SDMT Nucleo Diga di Camastra





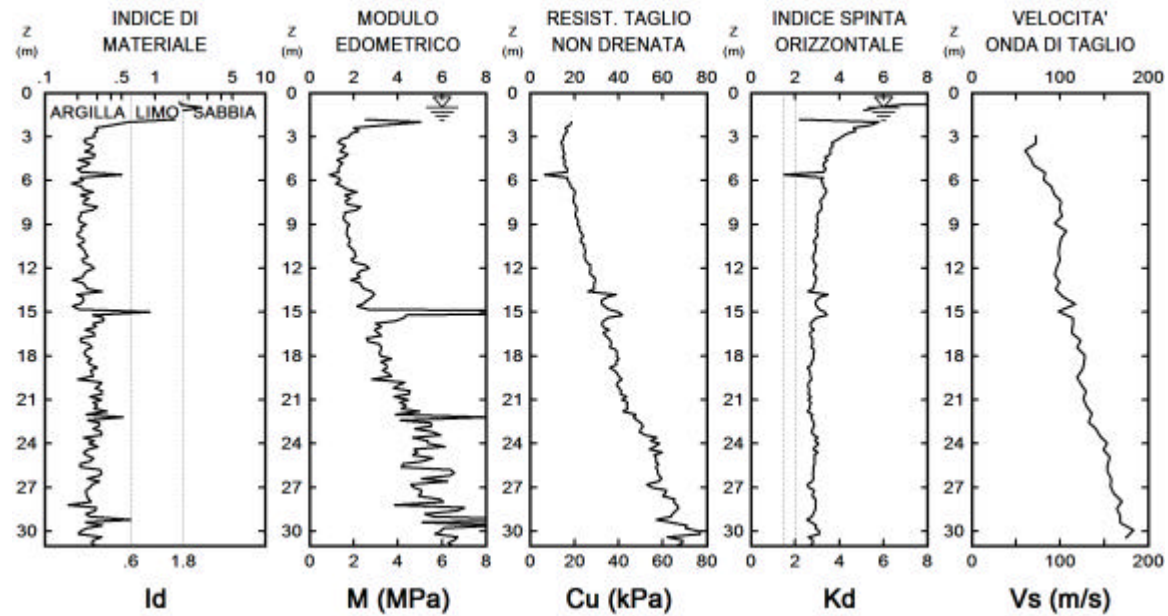
SDMT a Cassino FFSS alta velocità





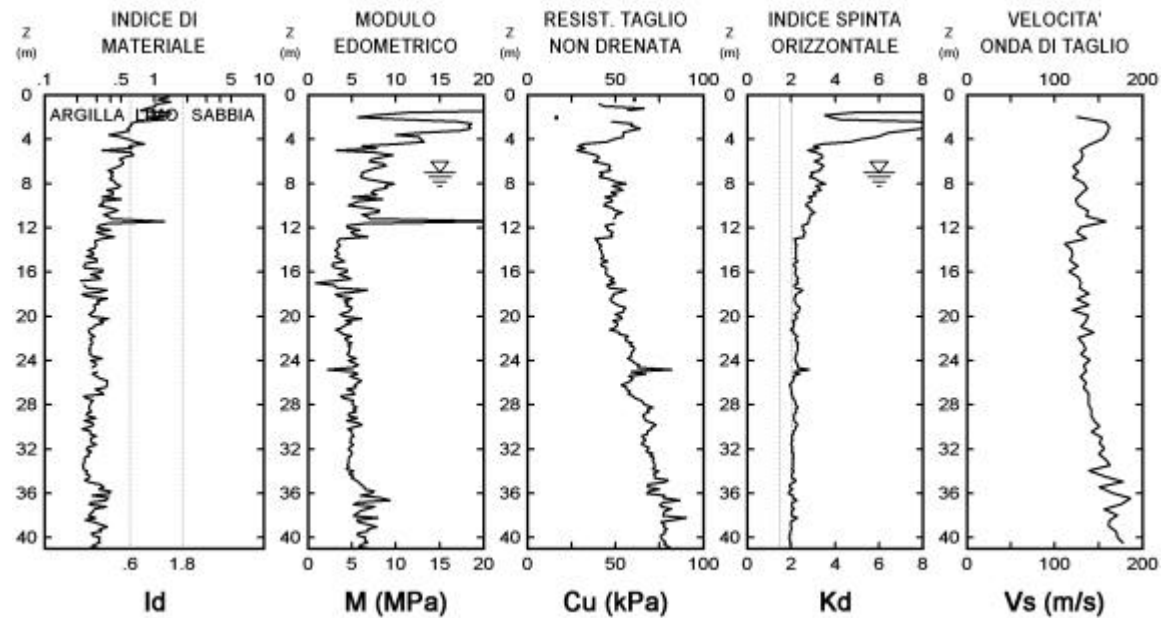
SDMT Fucino

Centro Telespazio





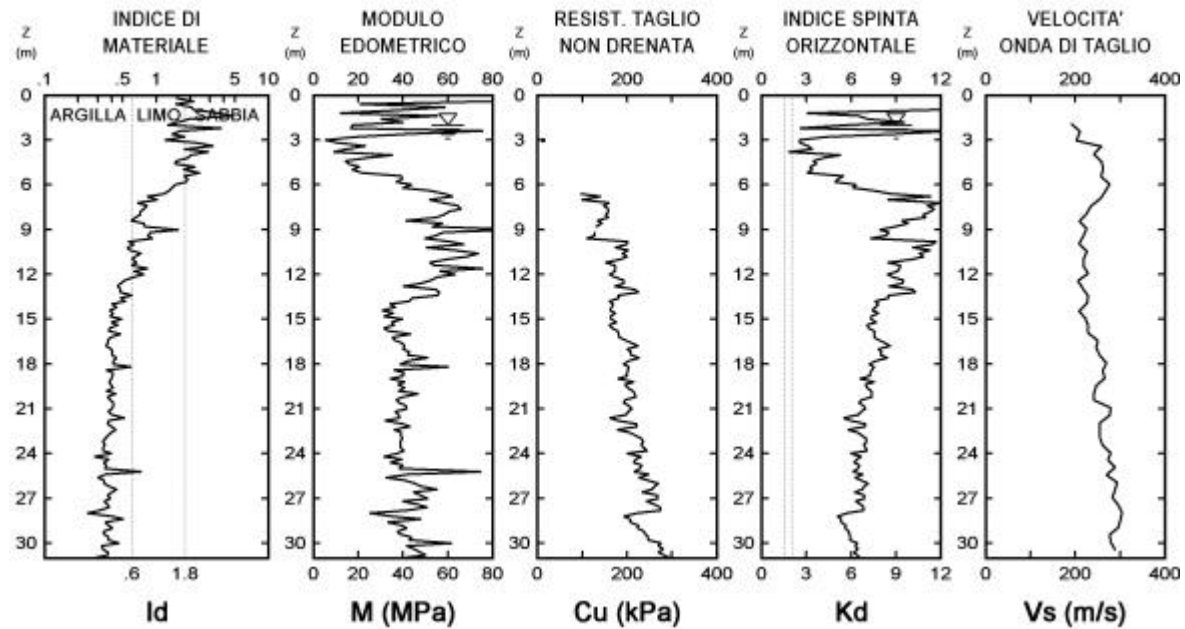
SDMT ST Microelectronics CATANIA





SDMT

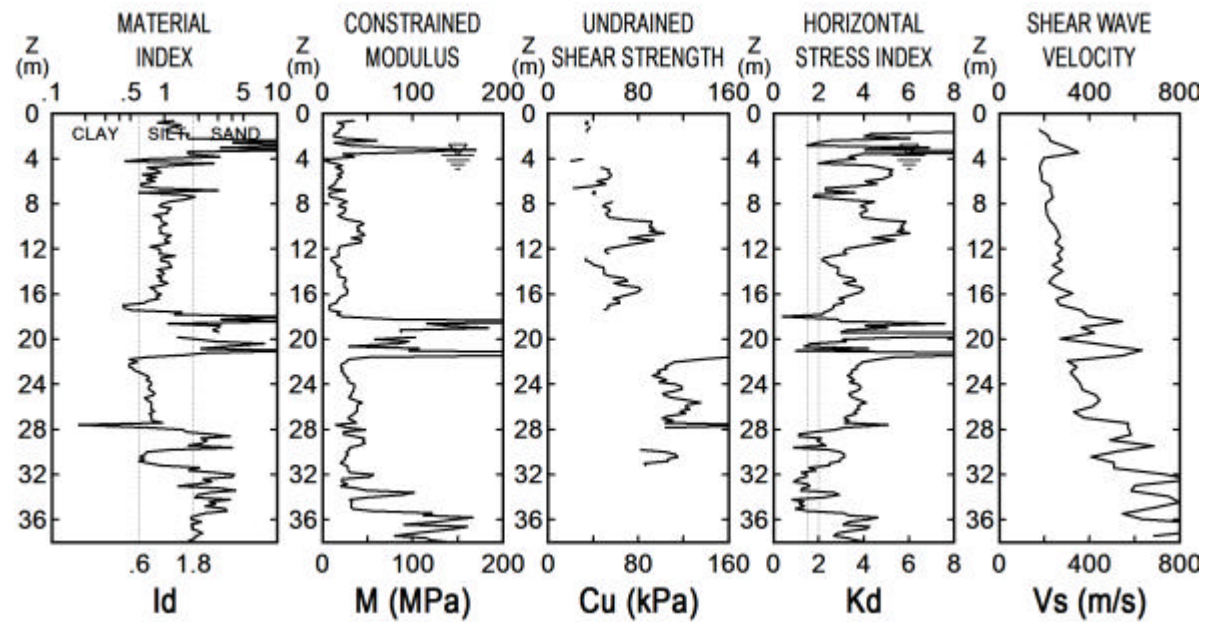
Villa Comunale Bellini di Catania





SDMT

Nuova Stazione FFSS Alta Velocita' Bologna

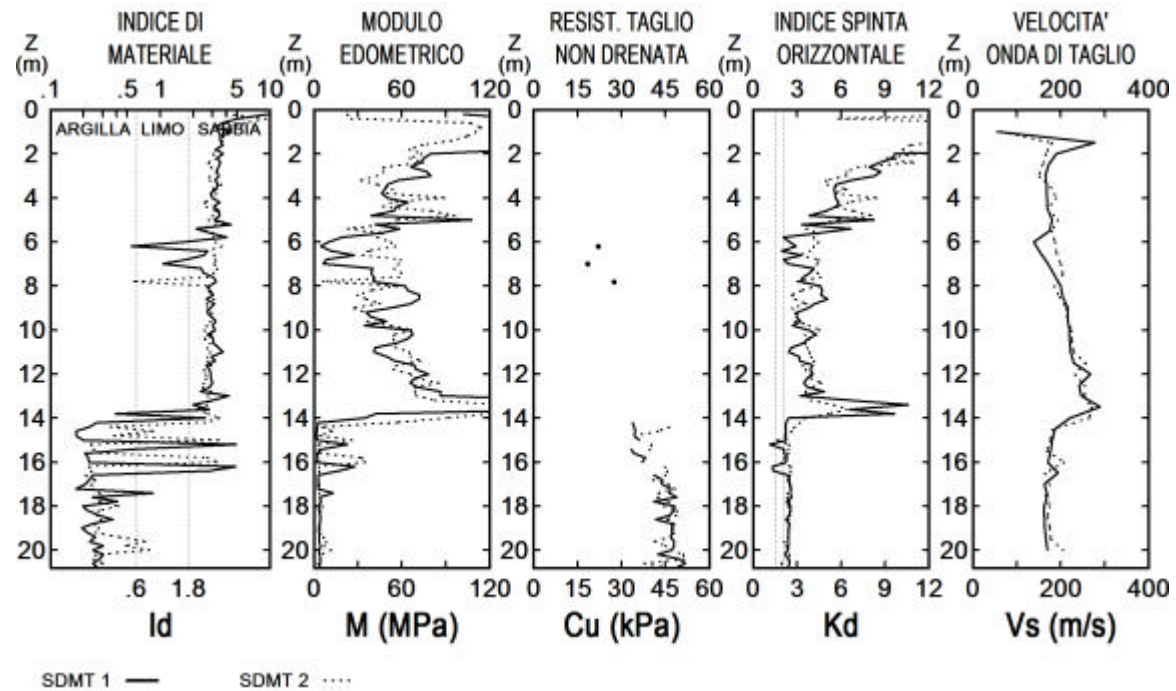




SDMT

Fiumicino – Roma

Feb 2005

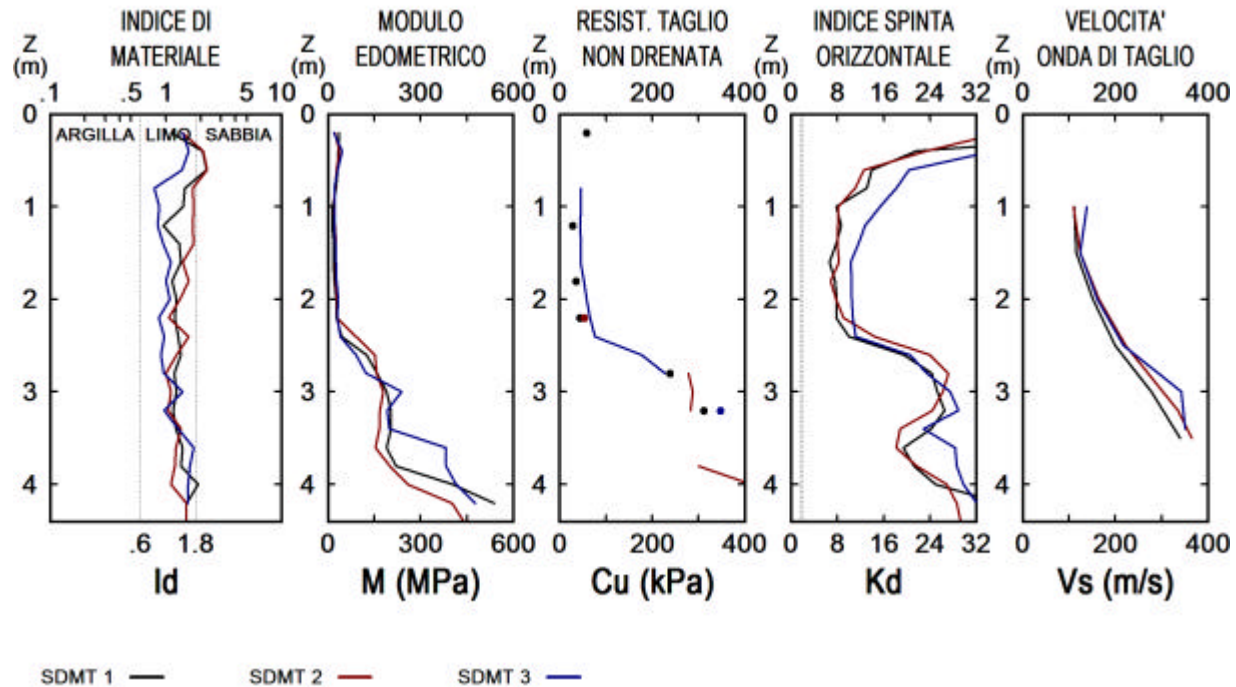




SDMT

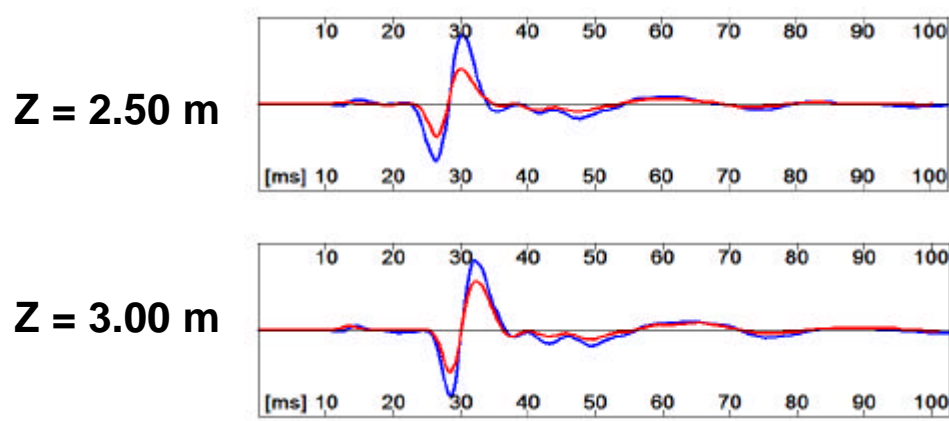
Casilino – Roma

Apr 2005



Prove SDMT Casilino

SDMT 1 - ripetibilità



| Z (m) | Vs (m/s) | | | | |
|-------|----------|-----|-----|-----|-----|
| | | | | | |
| 1.00 | 110 | 111 | 112 | 112 | 111 |
| 1.50 | 116 | 116 | 116 | 116 | |
| 2.00 | 152 | 152 | 152 | 152 | |
| 2.50 | 201 | 200 | 199 | 200 | 201 |
| 3.00 | 277 | 277 | 278 | 277 | 281 |
| 3.50 | 336 | 341 | 340 | 340 | 340 |

Attenuazione segnale:

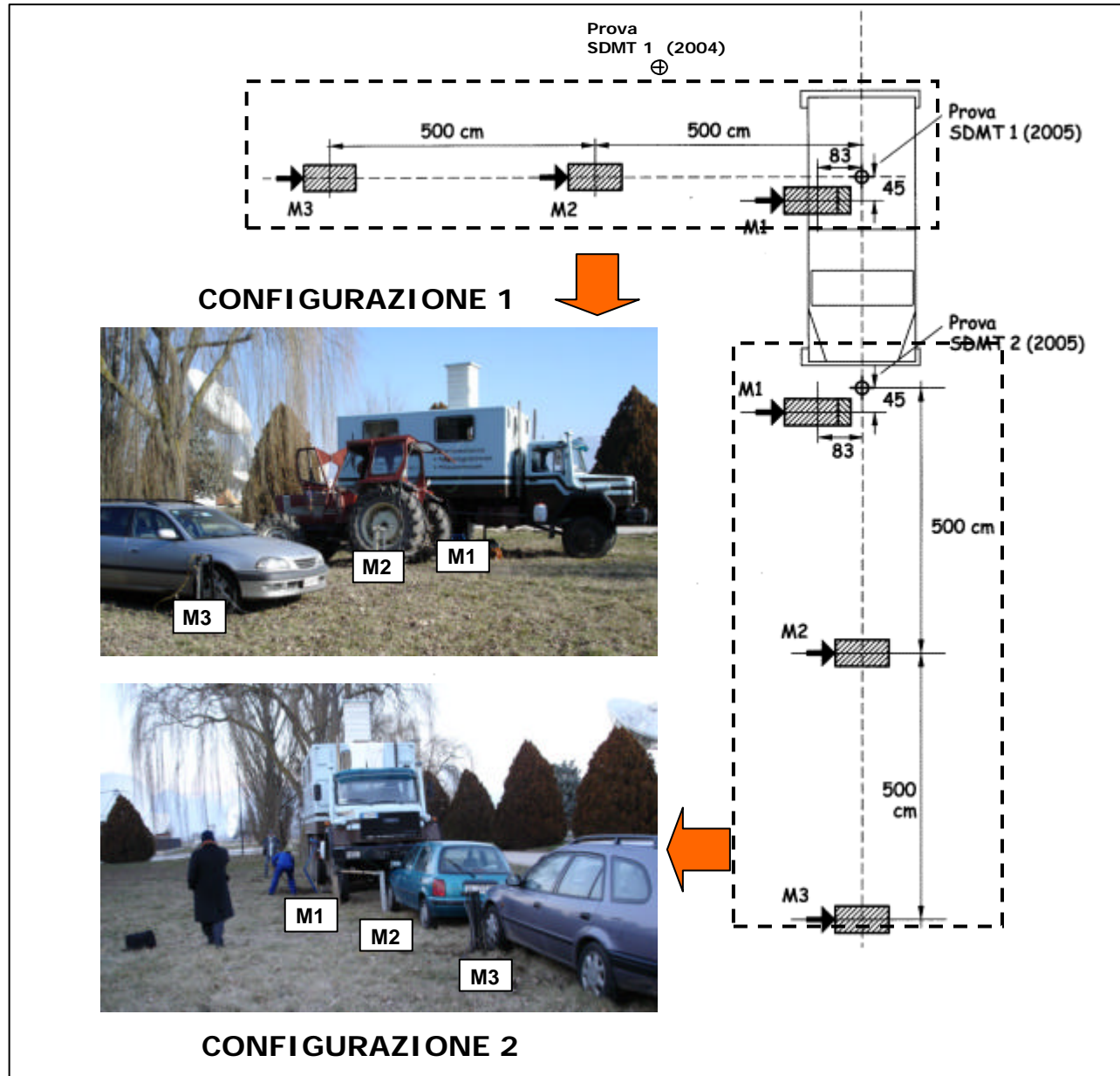
- Attenuazione geometrica
- Aumento di rigidezza
- Damping

Recommendation by Fahey

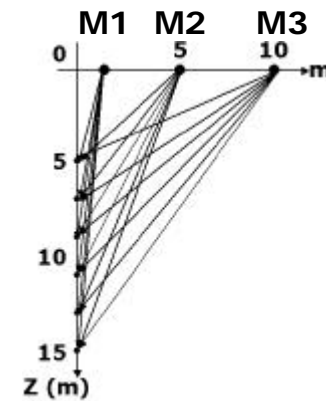
(Bali 2001)

- *“It is poor practice to perform penetration tests without Vs”*
- Perciò misuriamo Vs di routine
- Causa ordinanza, Enti (pubblici) richiedono Vs

Sorgenti a distanze diverse



Obliquità



Fucino – Telespazio
14 GEN 2004

LEGENDA

M1 = Martello 1

M2 = Martello 2

M3 = Martello 3