



REGIONE TOSCANA

Direzione Ambiente ed Energia
Settore Sismica Regionale - Prevenzione Sismica



CPT DATABASE OF THE TUSCANY REGION AND LIQUEFACTION RISK

Workshop on CPT test

Dr. Geol. Massimo Baglione – Settore Sismica

Pisa, 14 June 2019



Summary

- **Liquefaction Risk;**
- **Liquefaction hazard evaluation** for a 3rd Level Microzonation study in a high seismicity area of Central Italy: Case histories
- **CPT Database** of the Tuscany Region



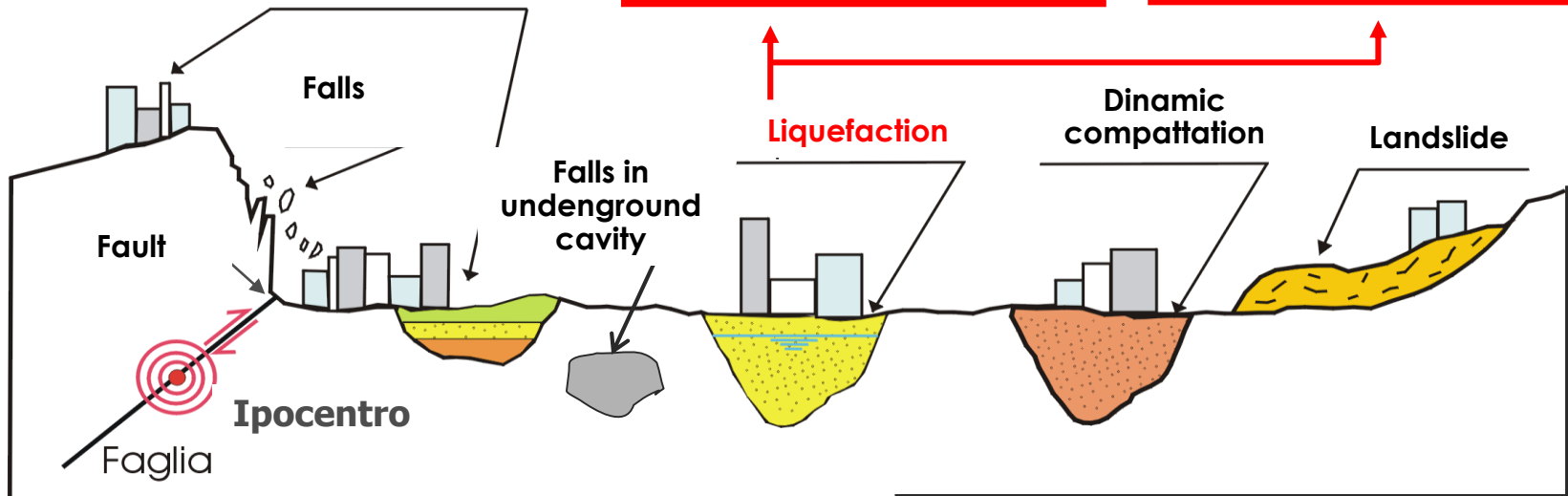
POSSIBLE SITE EFFECTS

Seismic Amplification



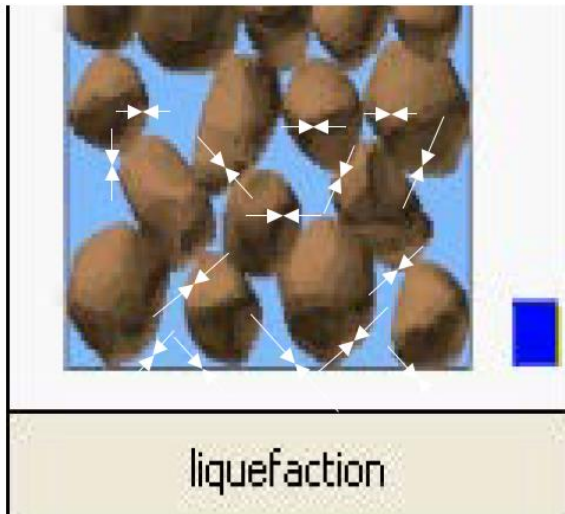
Site effects

Soil Failure





Soil liquefaction occurs when a saturated or partially saturated soil substantially loses strength and stiffness in response to an applied stress such as shaking during an earthquake or other sudden change in stress condition. As a consequence of pore pressure increase the soil becomes liquid.



Different types of liquefaction:

- Cyclic liquefaction;
- Cyclic mobility;
- Fluidification

$$\tau_f = \sigma' \cdot \tan \phi' = (\sigma - u) \cdot \tan \phi'$$

(Mohr-Coulomb failure criterion)



Examples of liquefaction phenomena

Southern Calabria (Italy) February 5, 1783 M7.3 earthquake



Friuli (Italy), May 6, 1976 M6.5 earthquake



(by courtesy of eng. Massimo Blasone – picture shot from geol. Livio Siro)

Sand boils



Examples of liquefaction phenomena

Niigata (Japan), June 16, 1964 M7.5 earthquake



(<http://nisee.berkeley.edu/eqjis.html>)

Izmit (Turkey), August 17, 1999 M7.4 earthquake



← loss of bearing capacity (shallow foundations)



(<http://nisee.berkeley.edu/eqjis.html>)

Cedimenti post-sismici



Examples of liquefaction phenomena

Christchurch (New Zealand), February 22, 2011 M6.2 earthquake





Examples of liquefaction phenomena

Emilia (Northern Italy), May 20, 2012 M6.1 earthquake



(by courtesy of V. Fioravante)

Emilia (Northern Italy), May 20, 2012 M6.1 earthquake



(by courtesy of V. Fioravante)

Emilia (Northern Italy), May 20, 2012 M6.1 earthquake

sand ejecta and sand boils @ San Carlo



Sand boils



Examples of liquefaction phenomena

Kaikoura (New Zealand), November 14, 2016 M7.8 earthquake



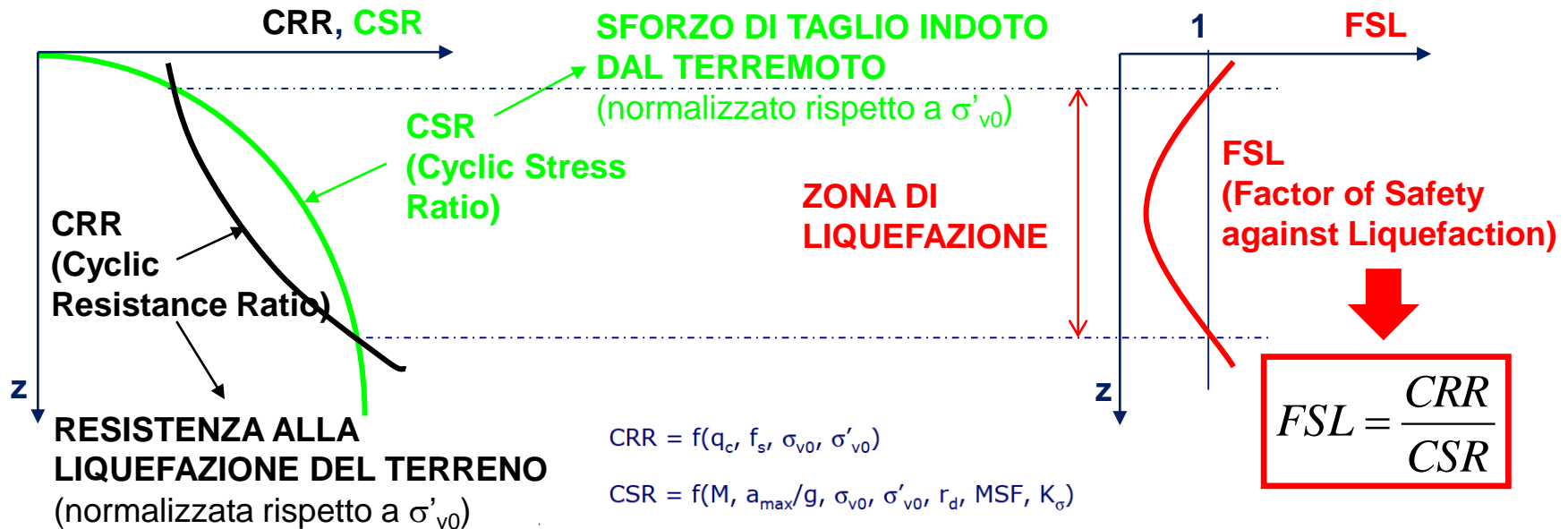
Aquila, 6 Aprile 2009 – M 5.8





Simplified methods for liquefaction estimation

Several simplified methods have been based on CPT results following both deterministic and probabilistic approaches (e.g. Robertson and Wride 1998; Juang et al. 2002, 2006; Cetin et al. 2004; Moss 2003; Moss et al. 2006; Idriss and Boulanger 2008; Robertson 2009, Boulanger and Idriss 2014).



Liquefaction risk, at a given site may be evaluated by Indexes like LPI (Liquefaction Potential Index)

$$LPI = \int_0^{z_{crit}} F(z) \cdot w(z) dz$$



Simplified methods for liquefaction estimation

z_{crit} : critical depth usually equal to 20m or even less (i.e. 15 or 10m). Liquefiable layers at depths greater than z_{crit} do not produce effects at ground level

$w(z)$: this function gives different weight to the occurrence of liquefaction at different depths

$$w(z) = \frac{200}{z_{crit}} \cdot \left(1 - \frac{z}{z_{crit}}\right)$$

$$LPI = \int_0^{z_{crit}} F(z) \cdot w(z) dz$$

$F(z)$: depends on the Liquefaction Safety Factor (FSL) with values in between 0 and 1

$$F(z) = \begin{cases} 0 & \text{per } FSL \geq 1.2 \\ 2 \cdot 10^6 \cdot \exp\left[-18.427 \cdot FSL(z)\right] & \text{per } 0.95 < FSL < 1.2 \\ 1 - FSL(z) & \text{per } FSL \leq 0.95 \end{cases}$$

Liquefaction Risk (Sonmez, 2003)

LPI	rischio di liquefazione
$\cong 0$	nullo
$0 < LPI \leq 2$	basso
$2 < LPI \leq 5$	moderato
$5 < LPI \leq 15$	alto
$LPI > 15$	molto alto

Liquefaction risk evaluation based on LPI ($z_{crit} = 20$ m)

Il calcolo di FSL è escluso per gli strati giudicati non liquefacibili da un punto di vista fisico ($z > z_{crit}$, $z < z_w$), litologico (ad es. $I_c > 2.6$) o meccanico (ad es. $(q_{c1n})_{cs} > 160$).



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Liquefaction hazard evaluation for a 3rd Level Microzonation study in a high seismicity area of Central Italy: Case histories



Microzonation studies for liquefaction hazard generally cover **wide areas** and require many in situ tests performed at great density in order to gain more accurate estimate of the soil liquefaction potential.

CPTs are frequently preferred over other in situ tests used in evaluating soil liquefaction potential such as Standard Penetration Tests or in-hole/surface geophysical tests for shear wave velocity measurement.

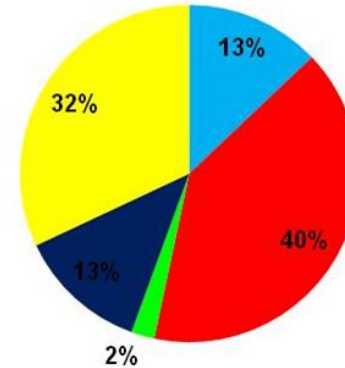
CPT-based approaches for liquefaction estimation are based on empirical relationships developed from worldwide seismic liquefaction case histories. The most recently compiled and widely used CPT-based methods refer to data obtained from electrical cone penetrometers or piezocones. However, it cannot be excluded that some early relationships for liquefaction evaluation are based on data collected using a mechanical cone. Electrical CPT-based methods applied to mechanical CPT data without any form of correction lead to erroneous estimates of liquefaction resistance and significantly non-conservative results. In fact, the sleeve friction, f_s , is affected by the greatest error when a mechanical penetrometer is used. Sleeve friction has the greatest influence on the fine content and plasticity index assessment and, consequently, on soil classification and liquefaction susceptibility estimation.



ANALISI E STUDI FINALIZZATI ALLA VERIFICA DELLA SUSCETTIBILITÀ A LIQUEFAZIONE DEI TERRENI NELL'AREA DEL MUGELLO

Convenzione stipulata tra Regione Toscana - Dir. Ambiente ed Energia - Settore Sismico Regionale Prevenzione Sismica e Università degli Studi di Firenze - Dipartimento di Ingegneria Civile e Ambientale (DICEA)

Gruppo di Lavoro:
Prof.ssa Ing. Claudia Madiati (Responsabile)
Dott. Ing. Johann Facciorusso
Dott.ssa Ing. Elisa Gargini
Prof. Ing. Giovanni Vannucchi



- Barberino di Mugello (29)
(18 CPTm, 11 CPTe)
- Borgo San Lorenzo (91)
- San Piero a Sieve (5)
- Scarperia (28)
- Vicchio (72)
(67 CPTm, 5 CPTe)

Distribuzione percentuale delle indagini CPT utilizzate

Database - 225 prove CPT

Liquefaction potential analyses were conducted extensively over the whole studied area (Mugello) to draw up liquefaction hazard maps and improve the previous 3rd level microzonation study. Soil liquefaction analyses were performed in more than **200 sites** over the whole studied Mugello area in terms of liquefaction potential and cumulated settlements using three different CPT-based simplified methods:

- Boulanger and Idriss (2014),
- Juang et al. (2006)
- Robertson (2009).

Two important aspects were taken into account in the assessment:

- The correction for the effects of fines content
- The correction of data from mechanical CPT's**



The **sleeve friction**, f_s , has the greatest influence on the fine content and the plasticity index assessment and, consequently, on soil classification and liquefaction susceptibility estimation. Furthermore, f_s is affected by the greatest error when a mechanical penetrometer is used. For these reasons, electrical CPT-based methods applied to mechanical CPT data without any form of correction lead to erroneous estimates of liquefaction resistance and significantly non-conservative results, especially in case of intermediate soils are considered. To this regard, a procedure for correcting mechanical CPT data and providing modified equations and curves for liquefaction resistance estimation by means of CPT-based simplified methods has been proposed by Facciorusso et al. (2017).

Correzione dei risultati delle prove CPT meccaniche:

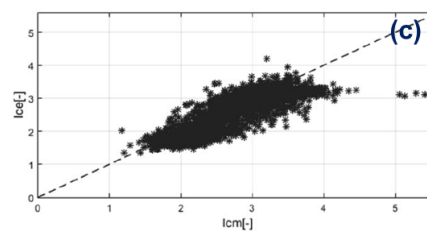
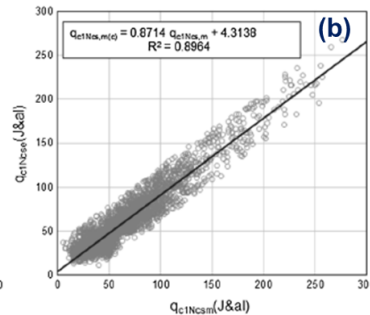
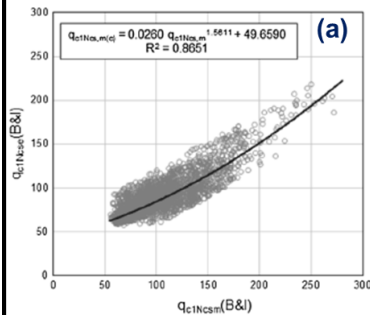
Per i metodi di B&I (2014) e J&al (2006) le grandezze $(q_{c1N})_{cs}$ ed I_c sono state corrette secondo le equazioni:

$$(q_{c1N})_{cs,EL} = 0.0260 \cdot (q_{c1N})_{cs,MEC}^{1.5611} + 49.6590 \quad (B\&I) \quad (a)$$

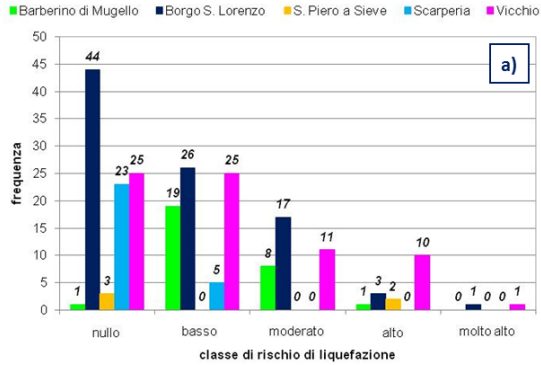
$$(q_{c1N})_{cs,EL} = 0.8714 \cdot (q_{c1N})_{cs,MEC} + 4.3138 \quad (J\&al) \quad (b)$$

$$I_{c,EL} = 0.9464 \cdot I_{c,MEC} \quad (c)$$

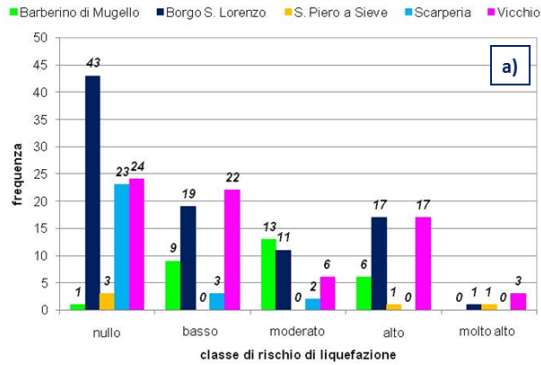
Facciorusso et al. (2017)



Regressioni di $(q_{c1N})_{cs,EL}$ rispetto a $(q_{c1N})_{cs,MEC}$ ottenute per i metodi di B&I (a) e J&al (b) e regressione di $I_{c,EL}$ rispetto a $I_{c,MEC}$ (c)

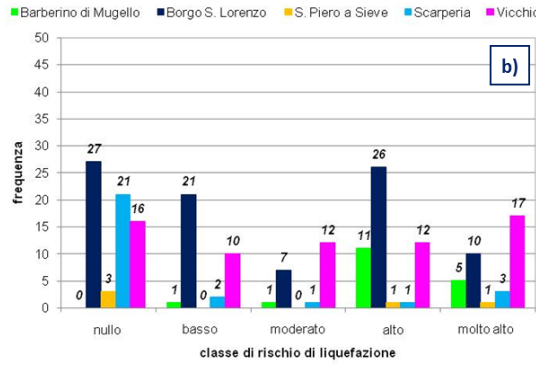


Boulanger e Idriss (2014) – SENZA CORREZIONE

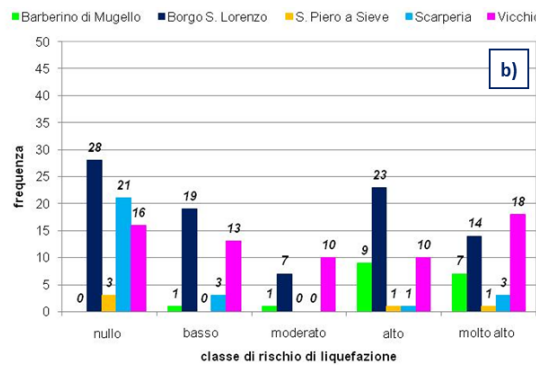


Juang et al. (2006) – SENZA CORREZIONE

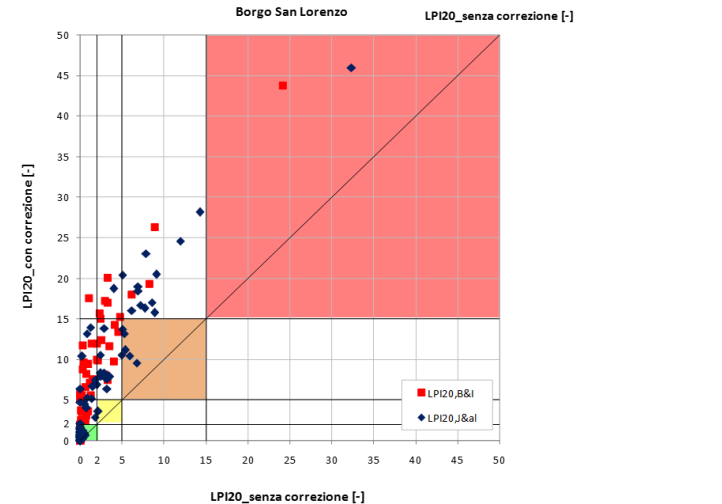
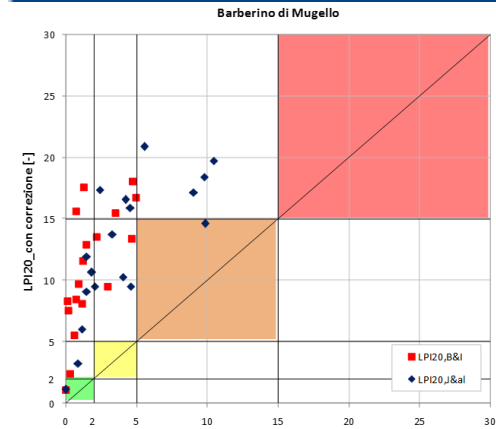
Da Madiati et alii, rapporto UNIFI-DICEA 2018



Boulanger e Idriss (2014) – CON CORREZIONE



Juang et al. (2006) – CON CORREZIONE



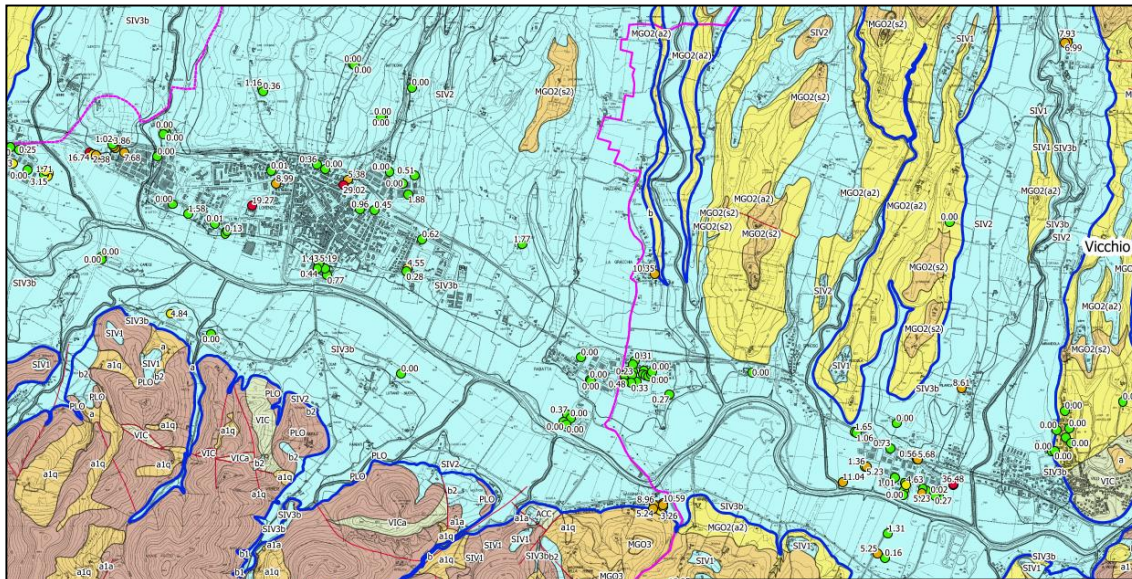
Good agreement between B&I 2014 and Juang et al. 2006 methodology



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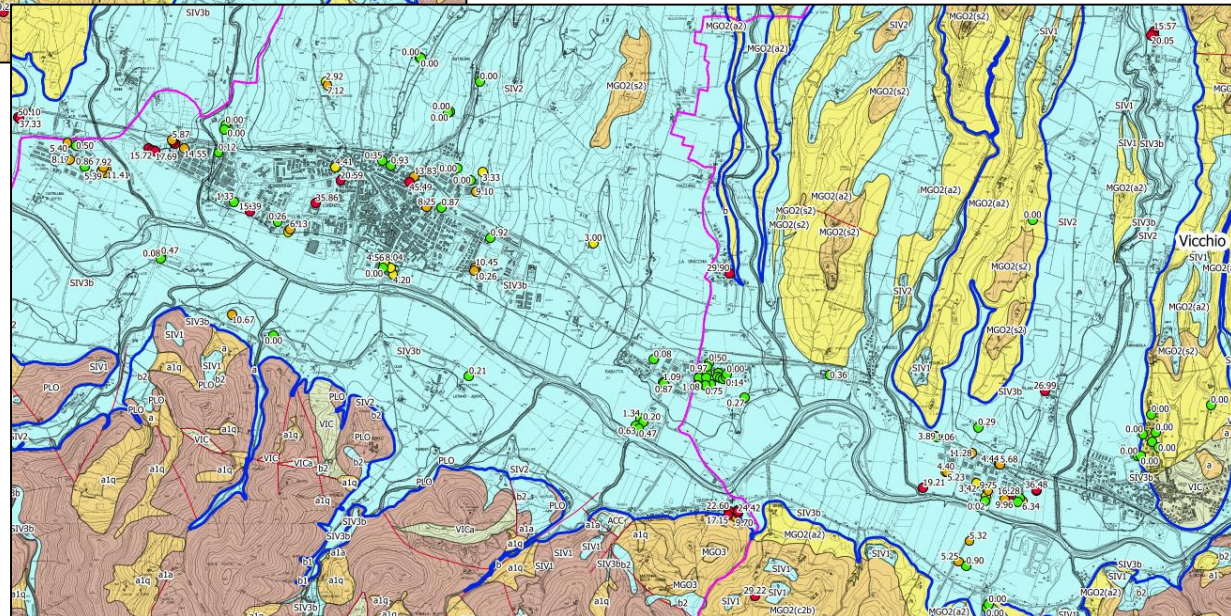
CASE HISTORIES n.1



Juang at al. 2006 - LPI uncorrected index

Map of liquefaction risk

Juang at al. 2006 - LPI corrected index



Indici LPI Juang & Alii

- *Indice da 0 a 2*
- *Indice da 2 a 5*
- *Indice da 5 a 15*
- *Indice maggiore di 15*







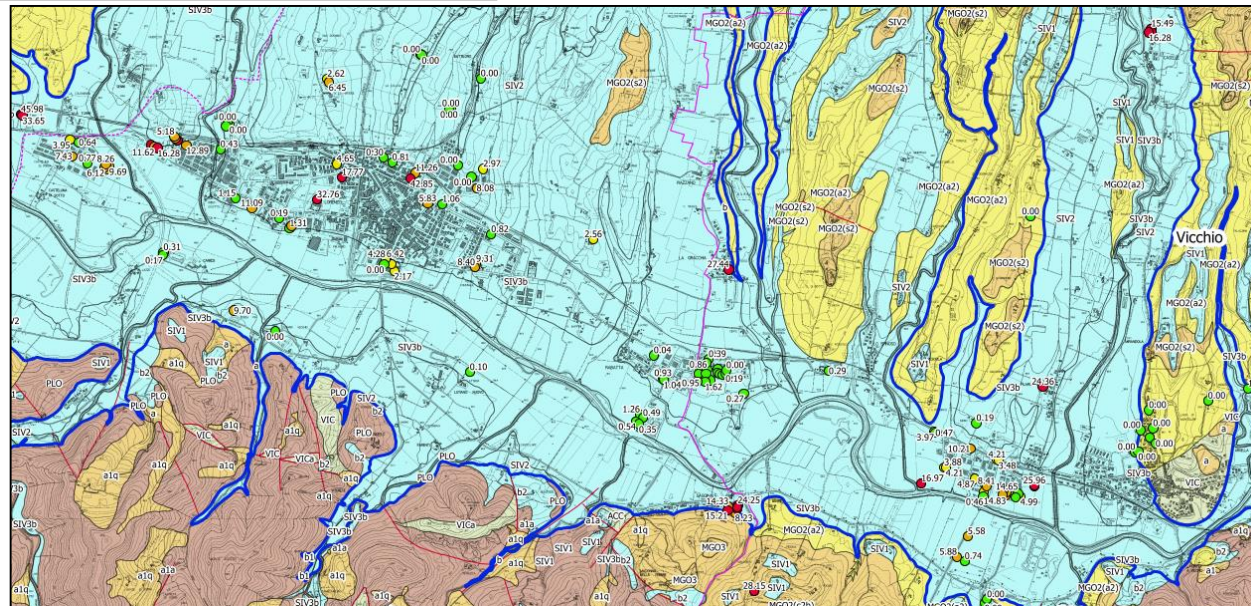
B & I 2014 - LPI uncorrected index

Map of liquefaction risk

B&I 2014 - LPI corrected index

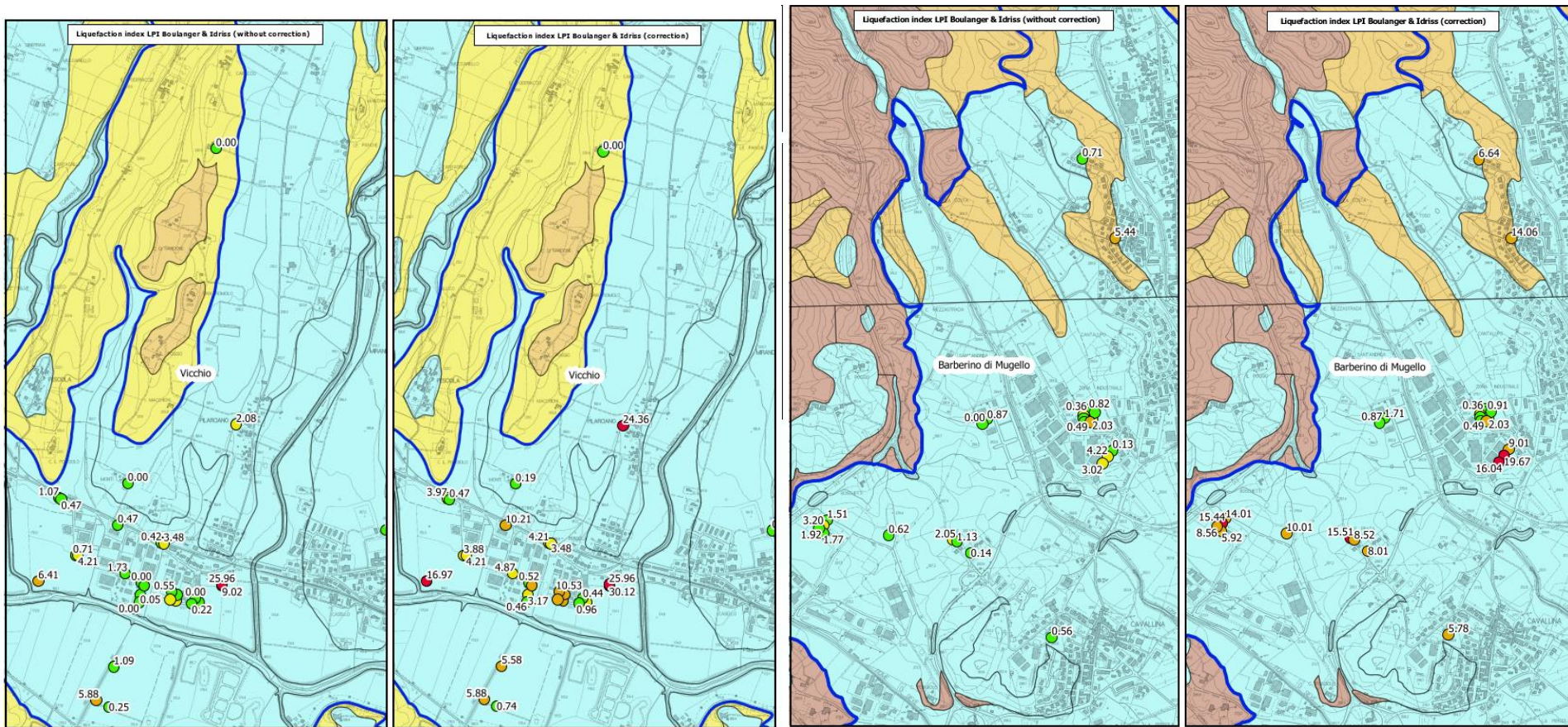
Indici LPI Boulanger & Idriss

-  *Indice da 0 a 2*
-  *Indice da 2 a 5*
-  *Indice da 5 a 15*
-  *Indice maggiore di 15*





Map of liquefaction risk



Maps of liquefaction hazard in terms of uncorrected and corrected LPI values provided for a test area in “Vicchio” and “Barberino” by using the **Boulangier and Idriss (2014)** method and assuming $I_c,lim = 2.6$.



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CASE HISTORIES n.2

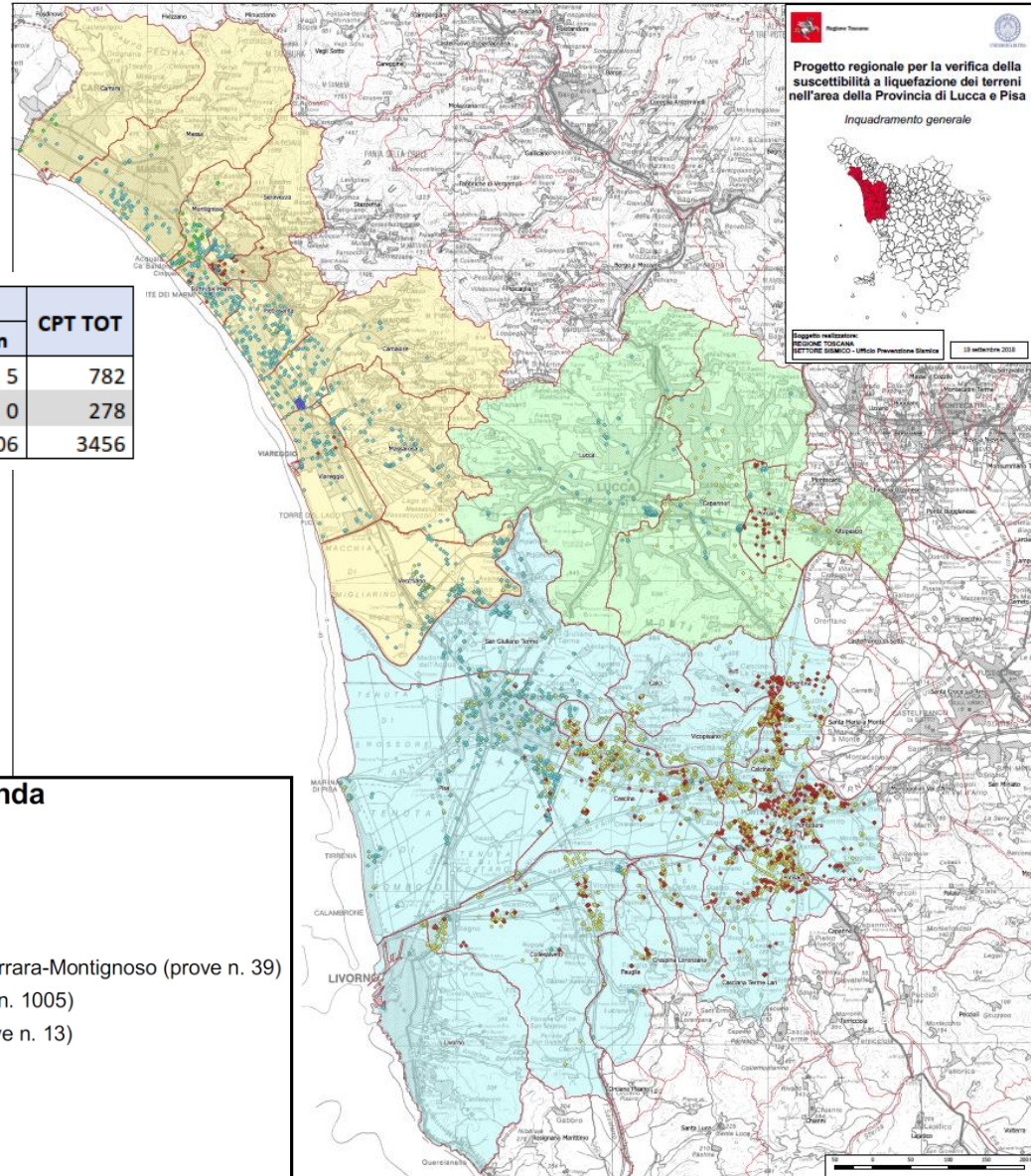


Regione Toscana



UNIVERSITÀ DI PISA

Progetto regionale per la verifica della suscettibilità a liquefazione dei terreni nell'area della Provincia di Lucca e Pisa



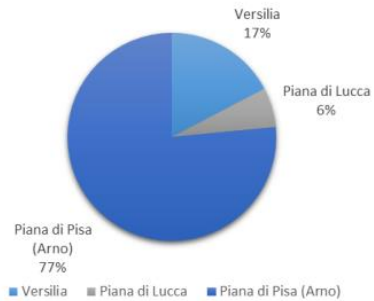
Progetto regionale per la verifica della suscettibilità a liquefazione dei terreni nell'area della Provincia di Lucca e Pisa
Inquadramento generale

Scalogramma realizzato:
REGIONE TOSCANA
SETTORE SISMICO - Ufficio Prevenzione Sismica
13 settembre 2018

Macroarea	Depth (m)						CPT TOT
	0-5 m	5-8 m	8-10 m	10-15 m	15-20 m	> 20 m	
Versilia	70	246	267	138	56	5	782
Piana di Lucca	58	111	68	33	8	0	278
Piana di Pisa (Arno)	156	561	1691	592	250	206	3456

Da Lo Presti et alii, rapporto UNIP-DICI 2018

CPT-Macroaree



Legenda

Fonte archivio indagini CPT

- DB Lamma (prove n. 1963)
- DB Provincia (prove n. 1523)
- DB Microzonazione Massa-Carrara-Montignoso (prove n. 39)
- DB Lamma solo grafici (prove n. 1005)
- DB MS Regione Toscana (prove n. 13)
- confini comunali
- Sub progetto Versilia
- Sub progetto Lucca
- Sub progetto Pisa

Lo Presti et al. 2017

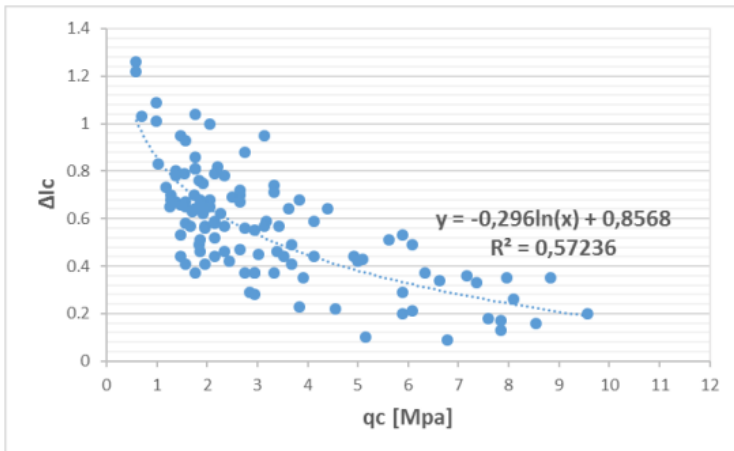


Soil liquefaction analyses were performed in more than 4000 sites over the “Versilia” area, “Pisa” Plan and “Lucca” area in terms of liquefaction potential (LPI) using three different CPT-based simplified methods, namely Boulanger and Idriss (2014), Juang et al. (2006) and Robertson-Write (1998).

Input parameters: Vn= 50 years; Cu=1; soil-type = C; different PGA for town; M=5.5

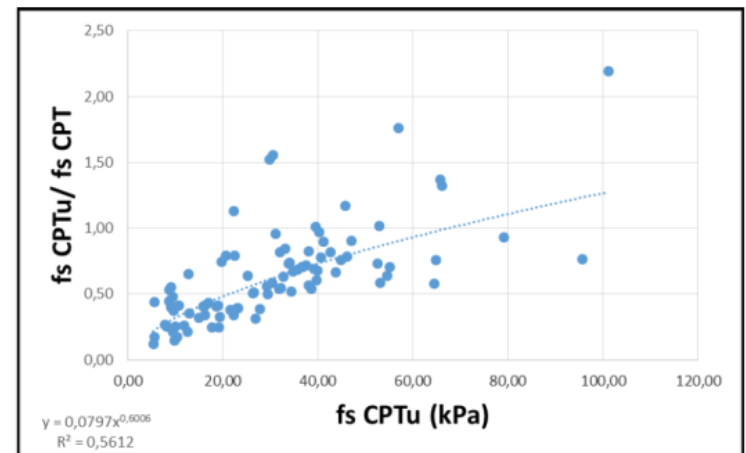
LPI valuation – Iwasaki et al. 1978

Ic correction (Meisina et al. 2017, Lo Presti et al. 2017) and correction (Francesconi, 2015)



$$\Delta I_c = -0.296 \ln(q_c) + 0.8568$$

$$I_c(\text{correct}) = I_c(\text{Robertson, 1990}) - \Delta I_c$$



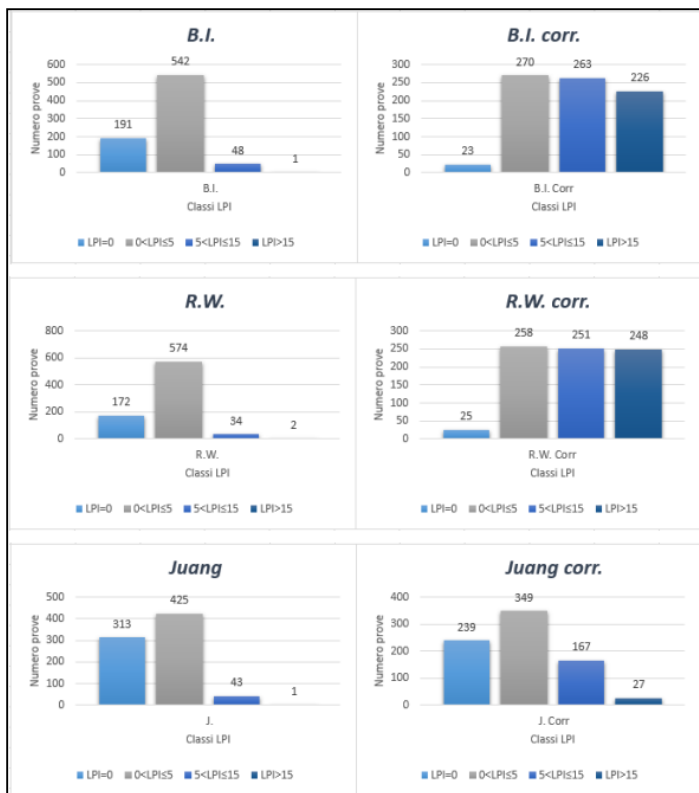
$$f_{s\ CPTu} = (0.0797 \times f_{s\ CPTm})^{2,504}$$



LPI - STATISTICAL DISTRIBUTION

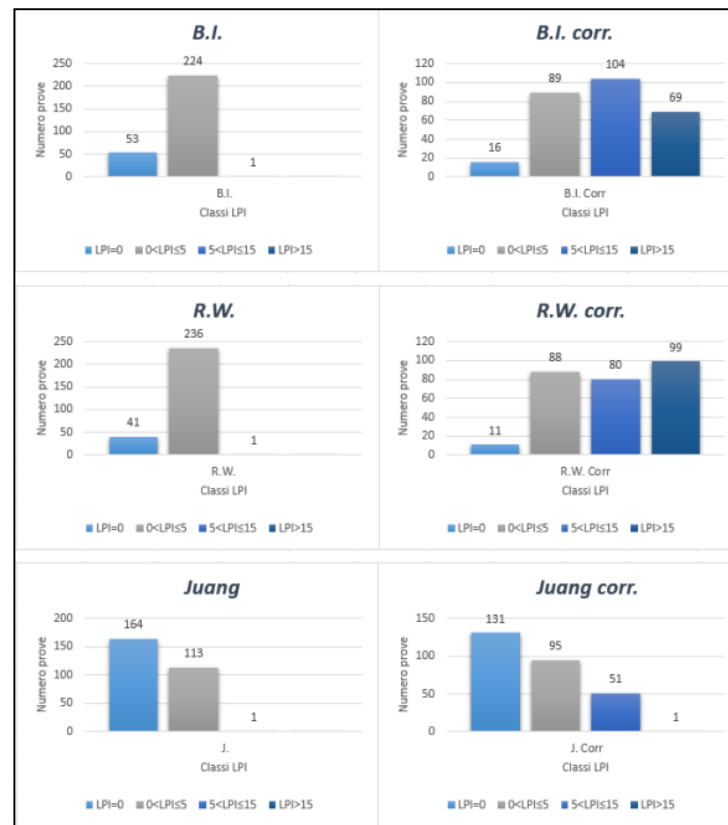
MACROAREA: VERSILIA

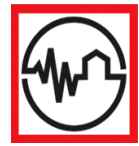
LPI Iwasaki	B.I.	B.I. Corr	R.W.	R.W. Corr	J.	J. Corr
LPI=0	191	23	172	25	313	239
0<LPI≤5	542	270	574	258	425	349
5<LPI≤15	48	263	34	251	43	167
LPI>15	1	226	2	248	1	27



MACROAREA: PIANA DI LUCCA

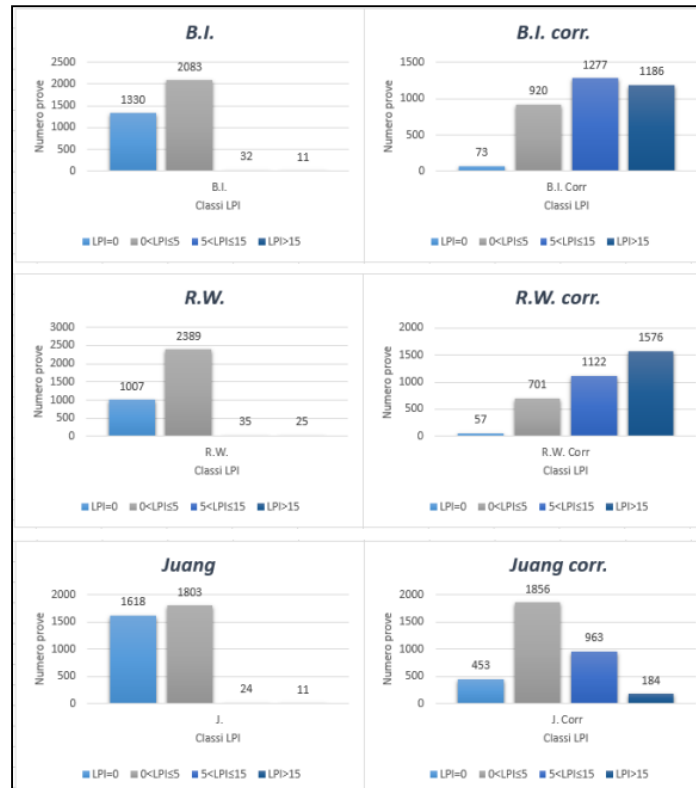
LPI Iwasaki	B.I.	B.I. Corr	R.W.	R.W. Corr	J.	J. Corr
LPI=0	53	16	41	11	164	131
0<LPI≤5	224	89	236	88	113	95
5<LPI≤15	1	104	1	80	1	51
LPI>15	0	69	0	99	0	1





LPI - STATISTICAL DISTRIBUTION

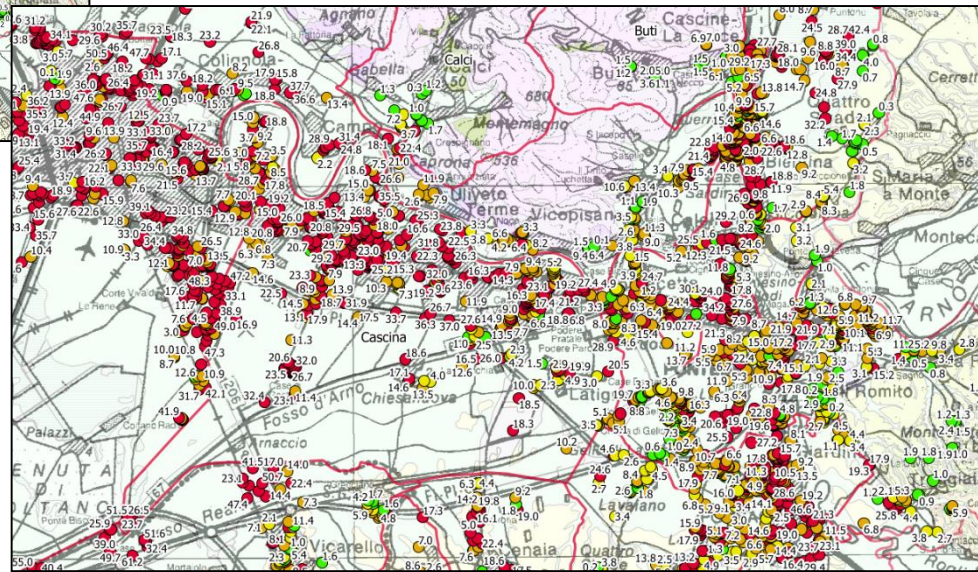
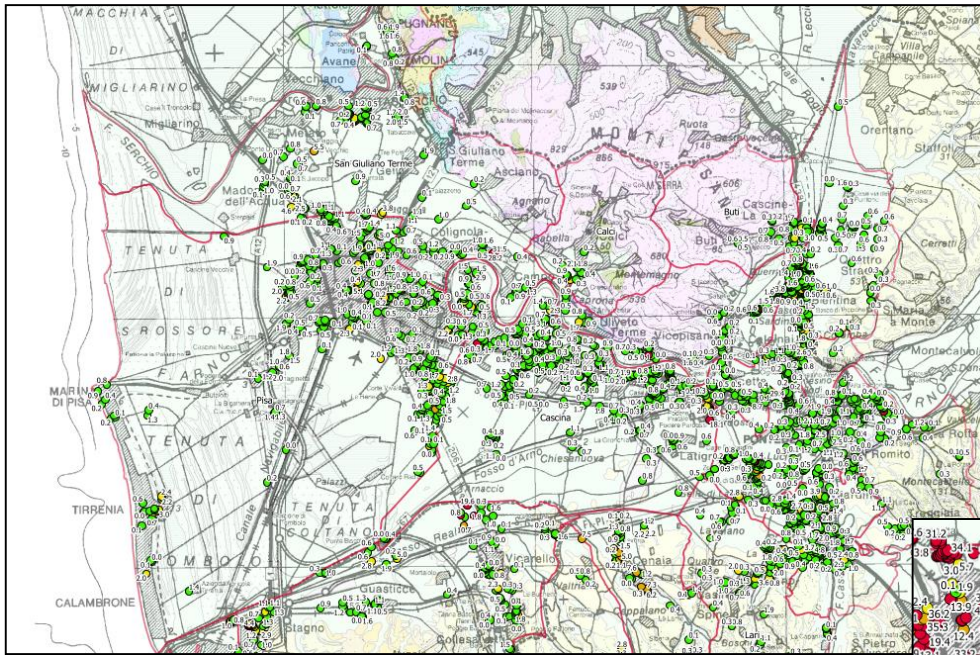
MACROAREA: PIANA DI PISA						
LPI <i>Iwasaki</i>	B.I.	B.I. Corr	R.W.	R.W. Corr	J.	J. Corr
LPI=0	1330	73	1007	57	1618	453
0<LPI≤5	2083	920	2389	701	1803	1856
5<LPI≤15	32	1277	35	1122	24	963
LPI>15	11	1186	25	1576	11	184





Map of liquefaction risk (Pisa plan)

LPI evaluation - Robertson-Write (1998)



Legenda

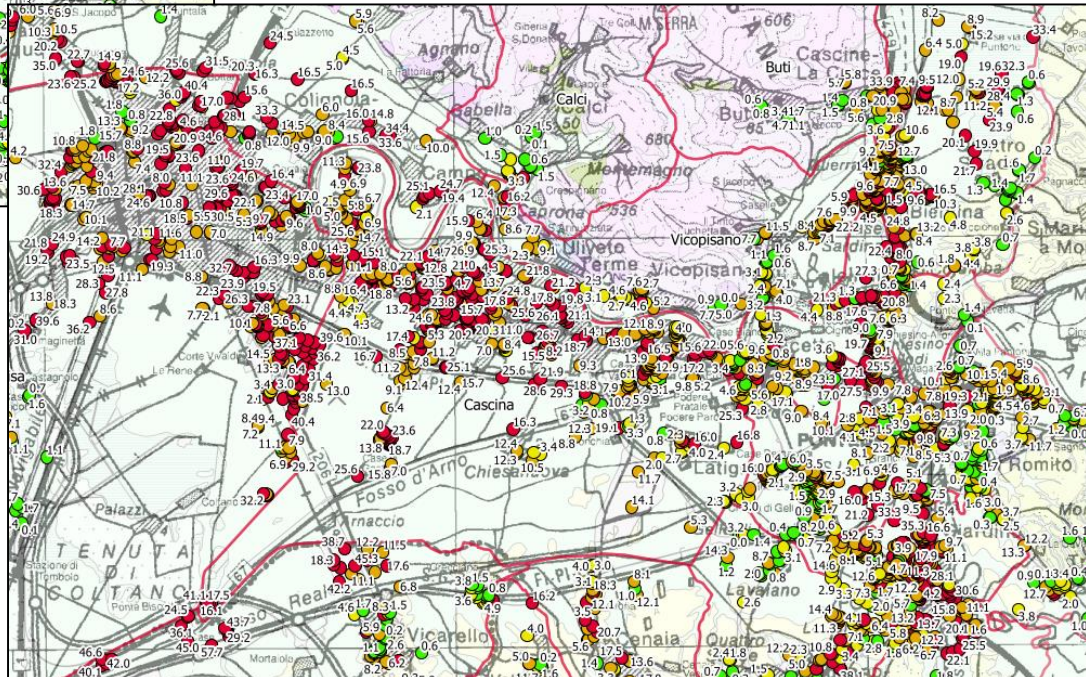
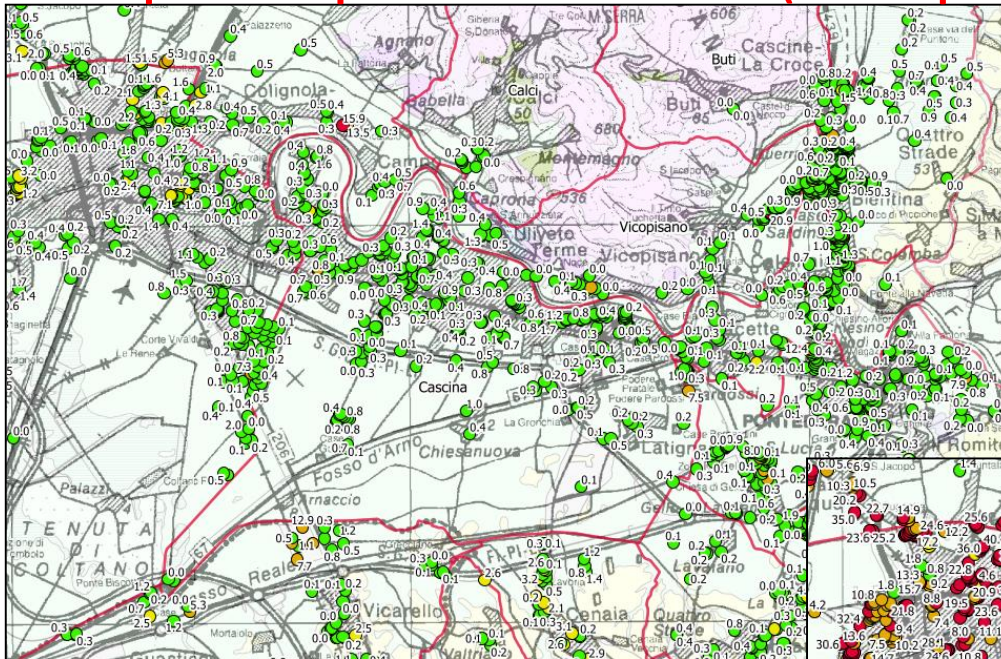
Classificazione LPI metodo R&W

- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15
- Sub progetto PISA



Map of liquefaction risk (Pisa plan)

LPI evaluation – Boulanger & Idriss (2014)



Legenda

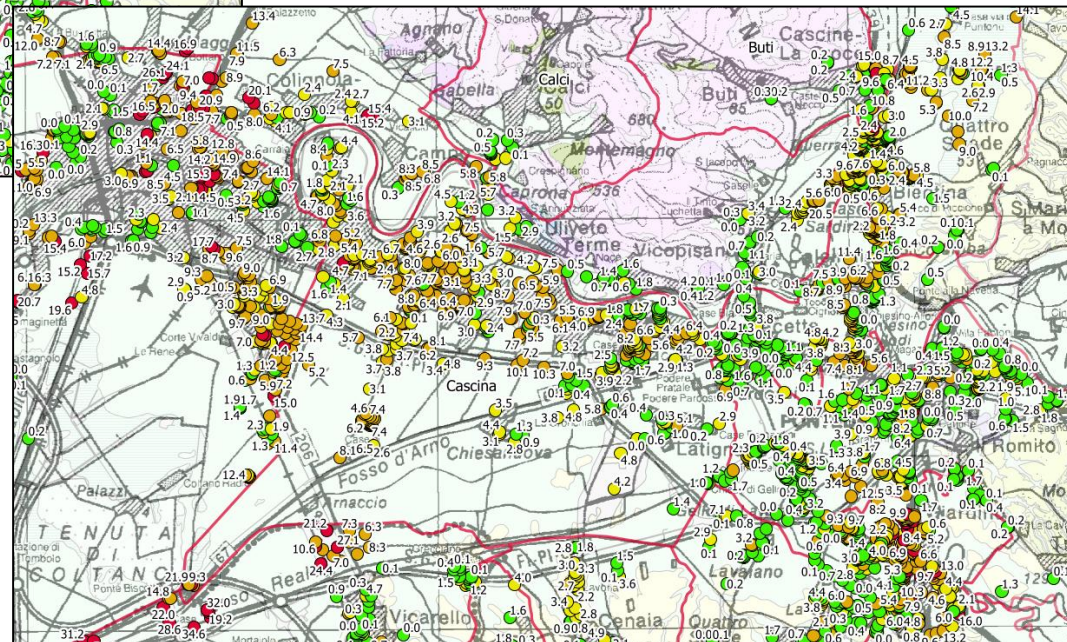
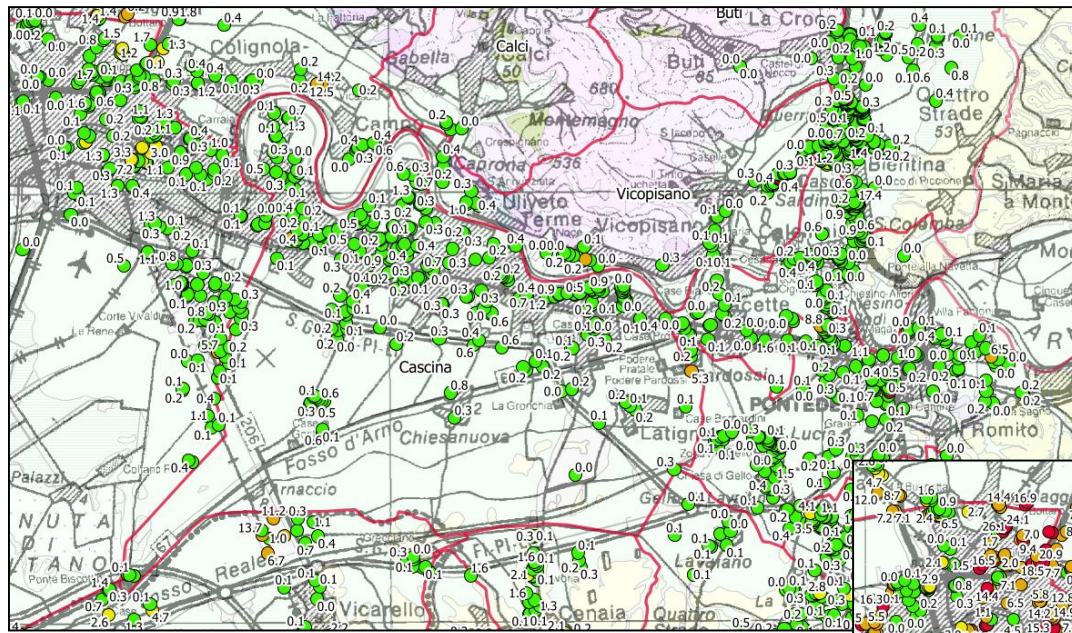
Classificazione LPI metodo B&I

- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15
- ▭ Sub progetto PISA



Map of liquefaction risk (Pisa plan)

LPI evaluation – Juang et al. (2006)



Legenda

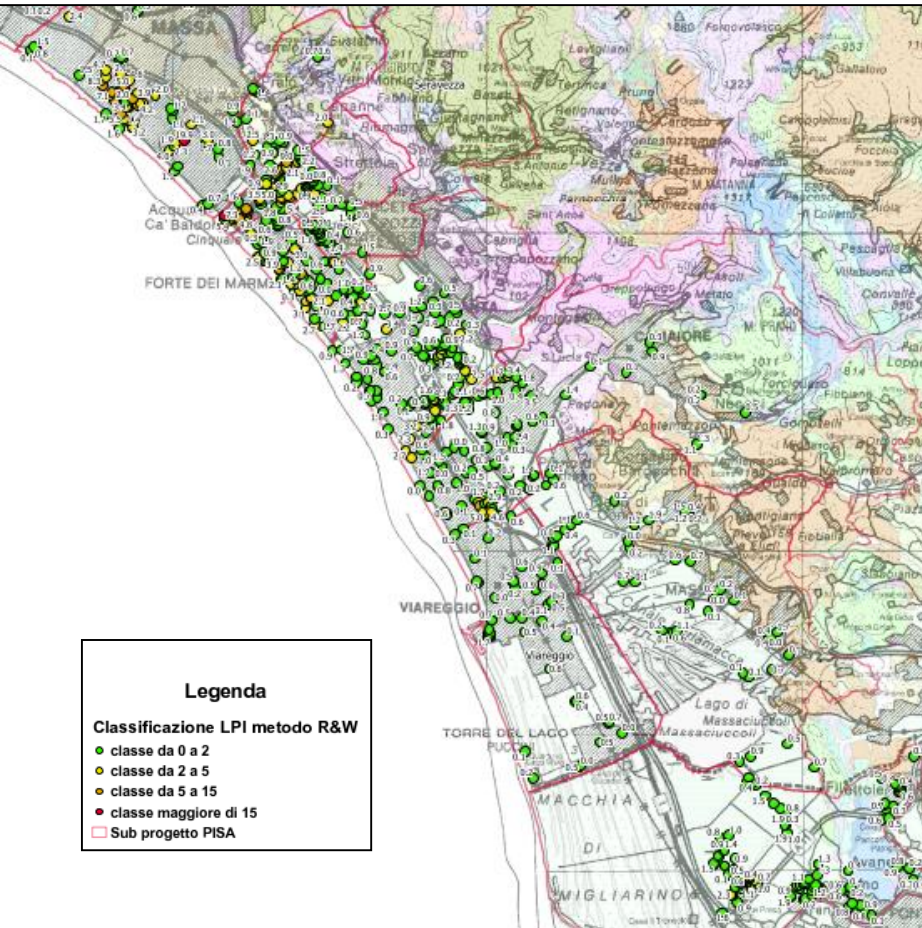
Classificazione LPI metodo J&AL

- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15

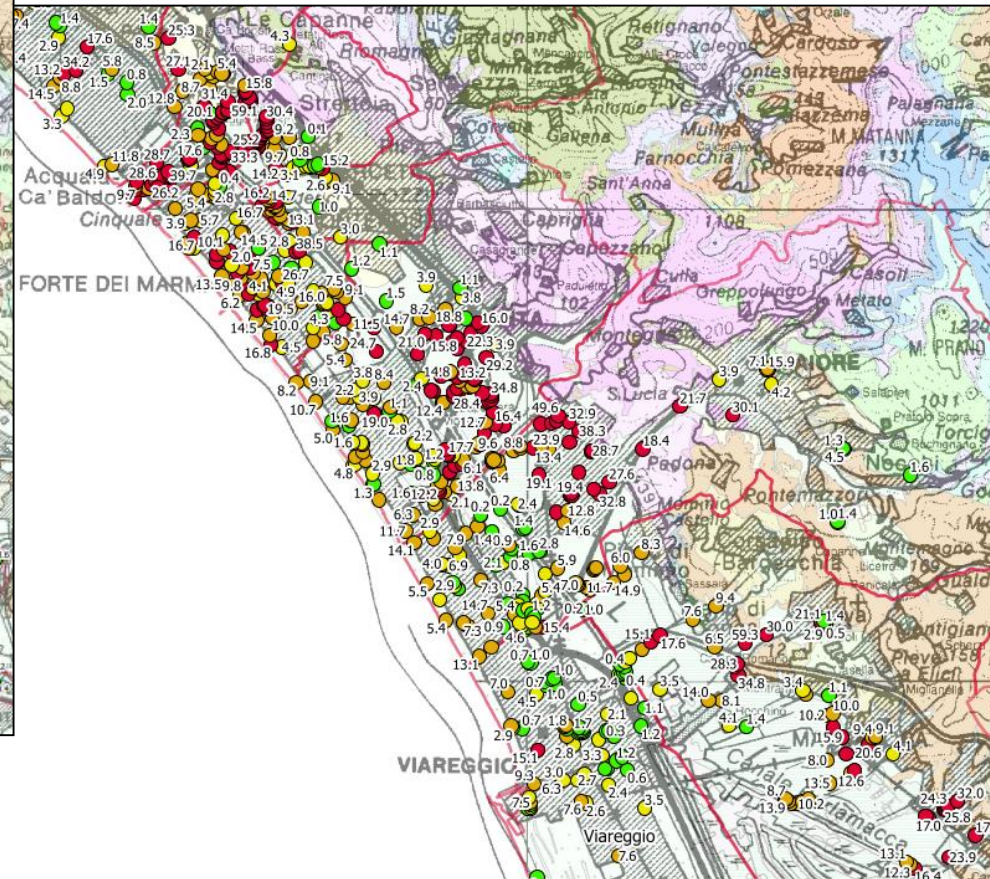
□ Sub progetto PISA



Map of liquefaction risk (Versilia area)

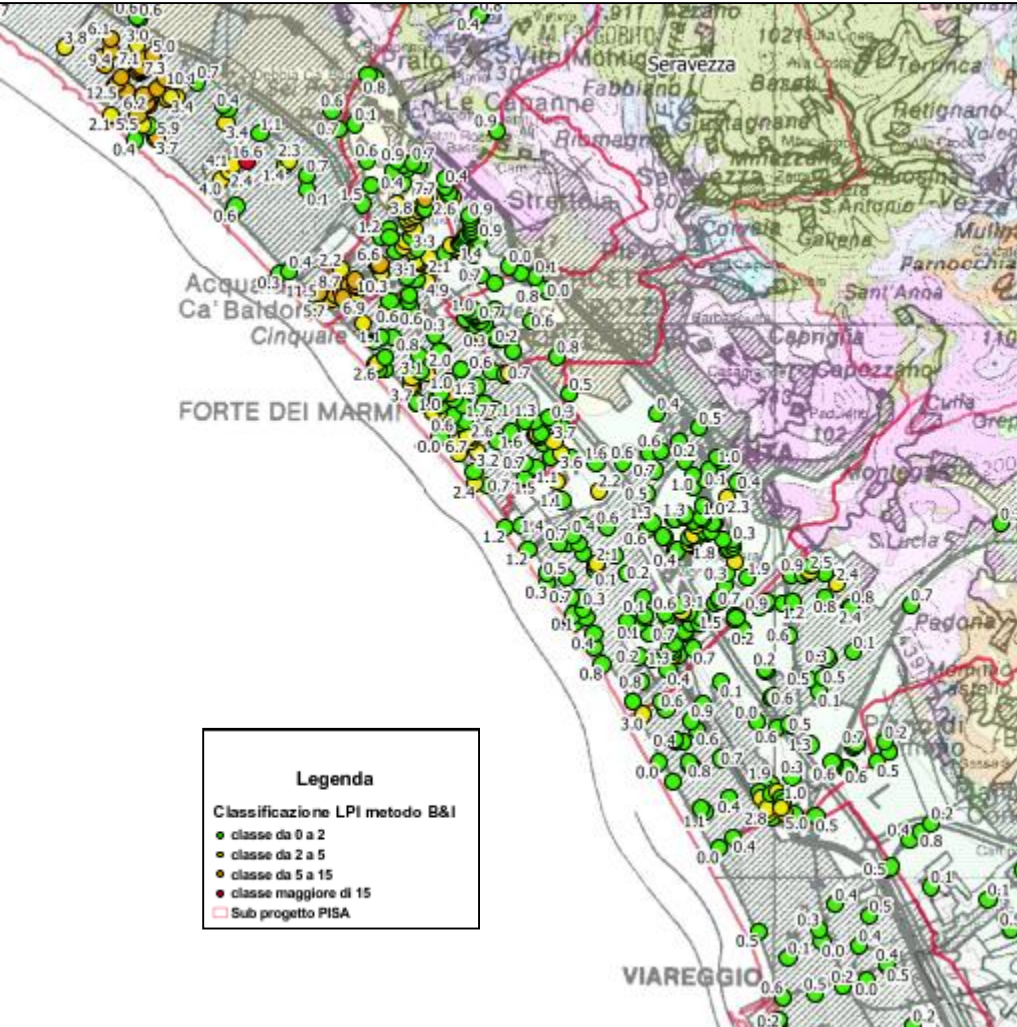


LPI evaluation - Robertson-Write (1998)

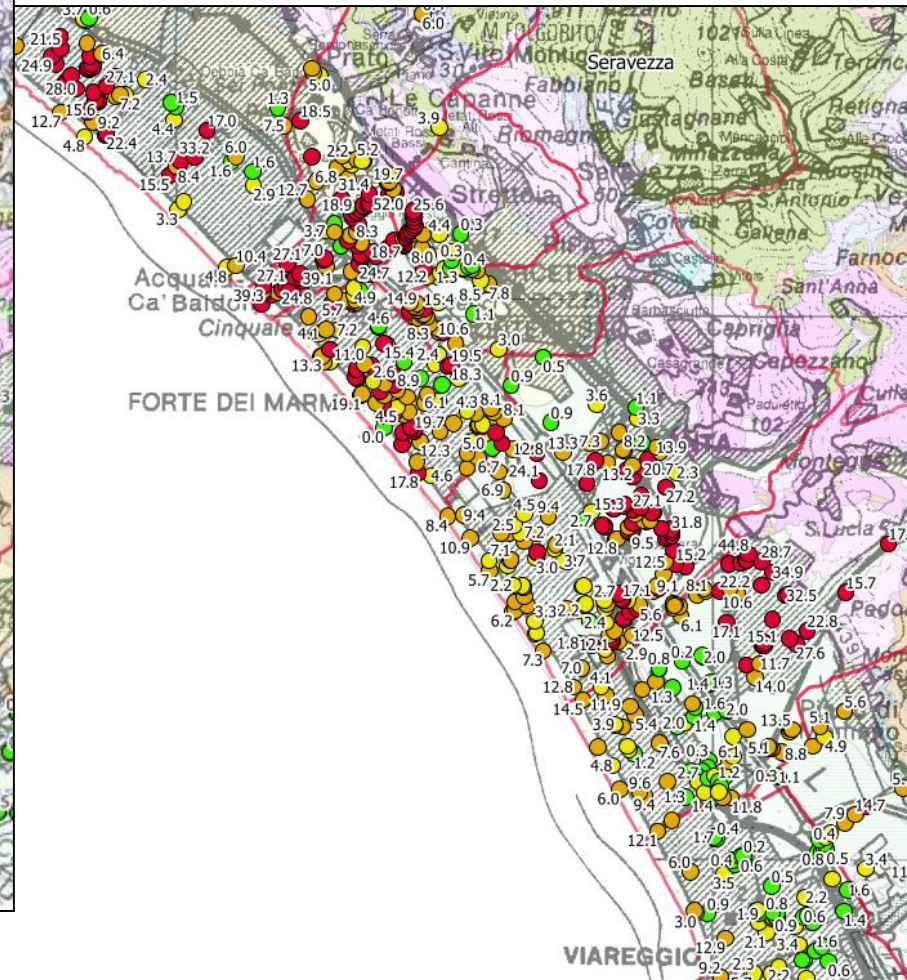




Map of liquefaction risk (Versilia area)



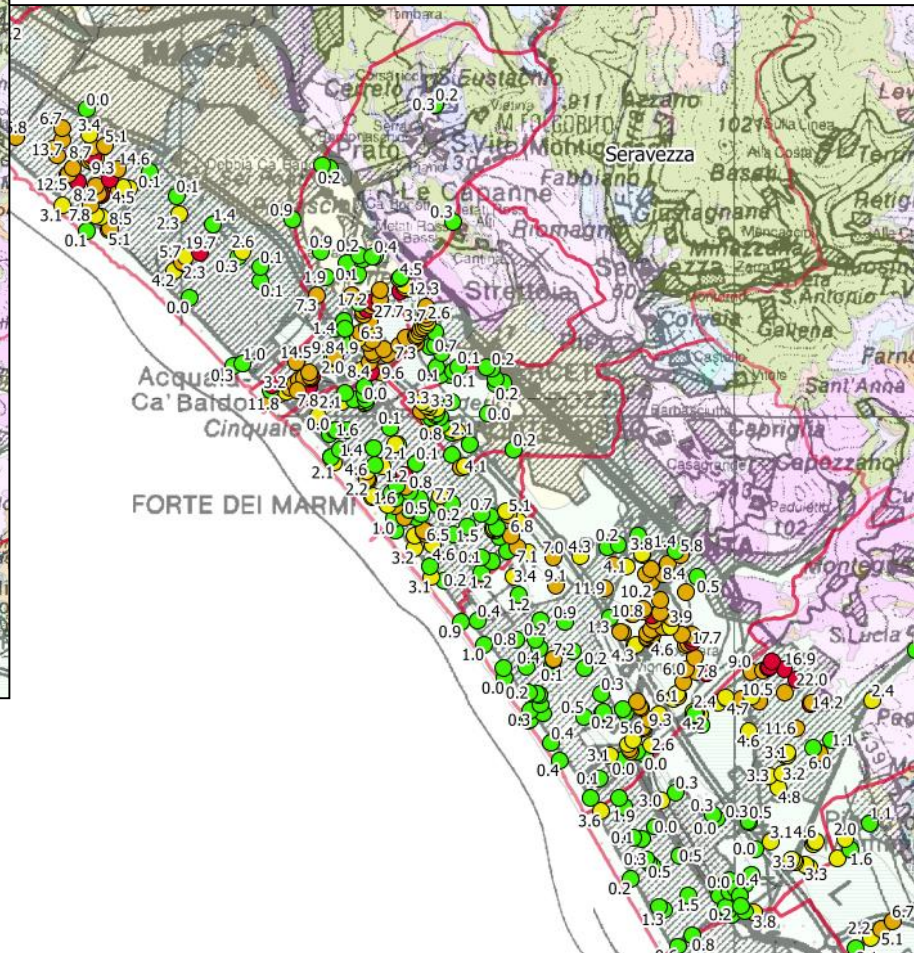
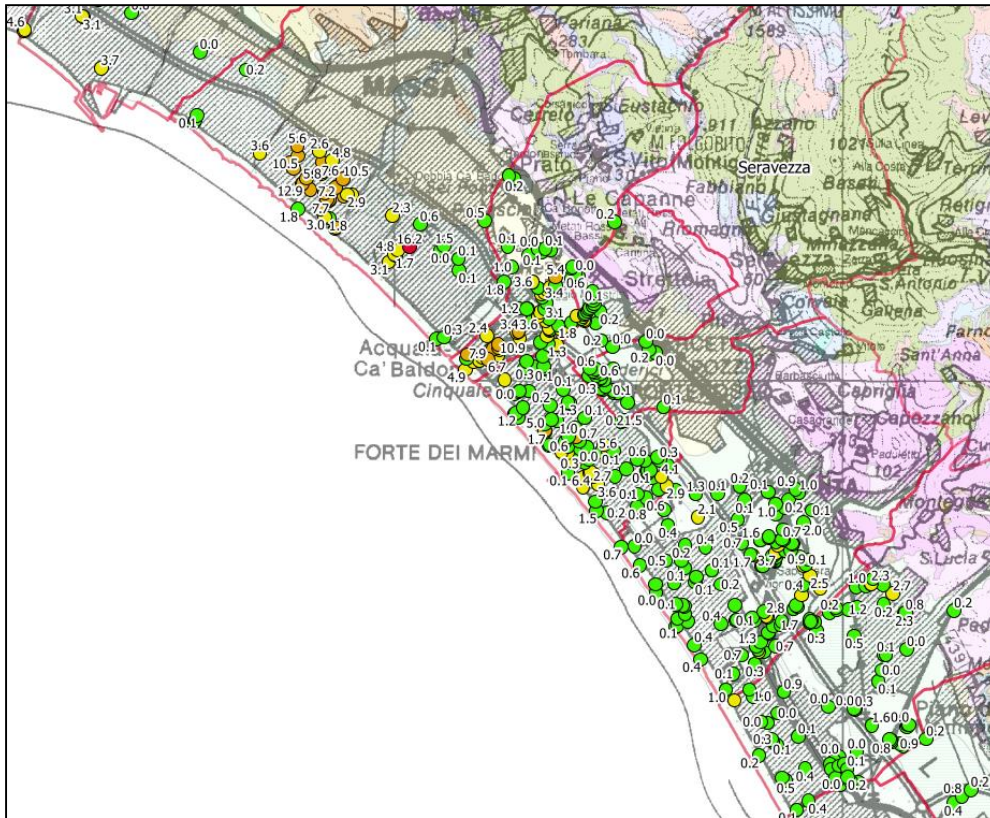
LPI evaluation – Boulanger & Idriss (2014)





Map of liquefaction risk (Versilia area)

LPI evaluation – Juang et al. (2006)



Legenda

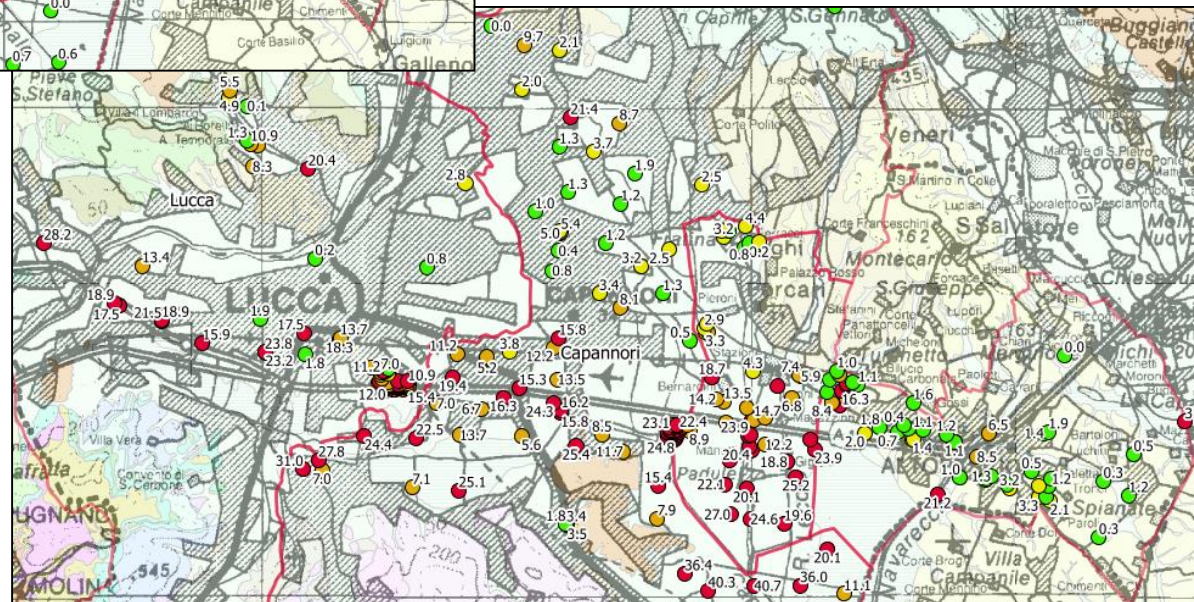
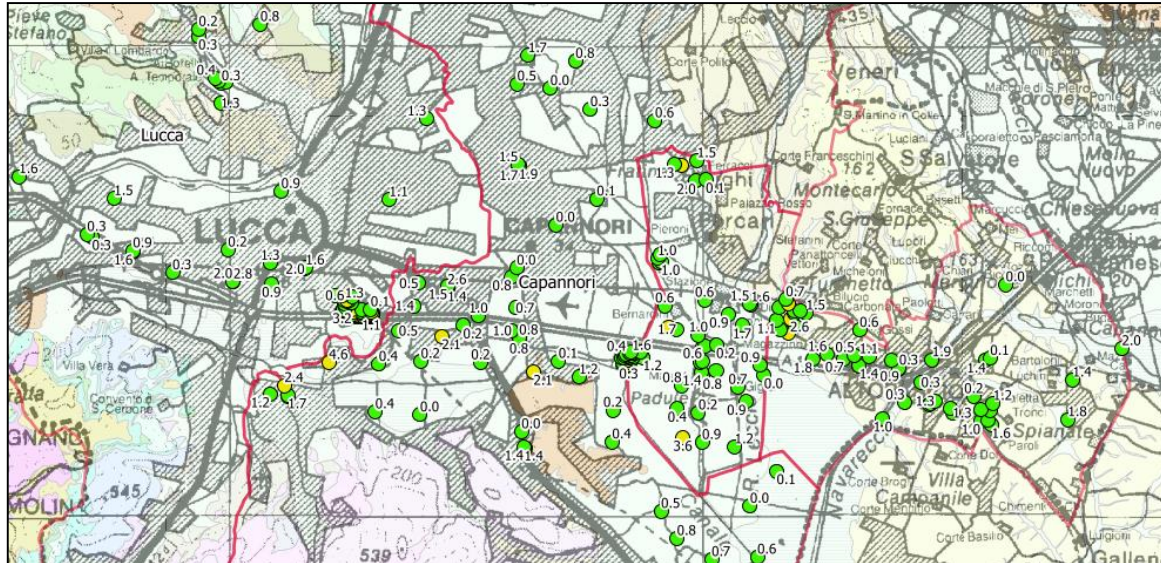
Classificazione LPI metodo J&A

- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15
- ▭ Sub progetto VERSILIA



Map of liquefaction risk (Lucca plan)

LPI evaluation - Robertson-Write
(1998)



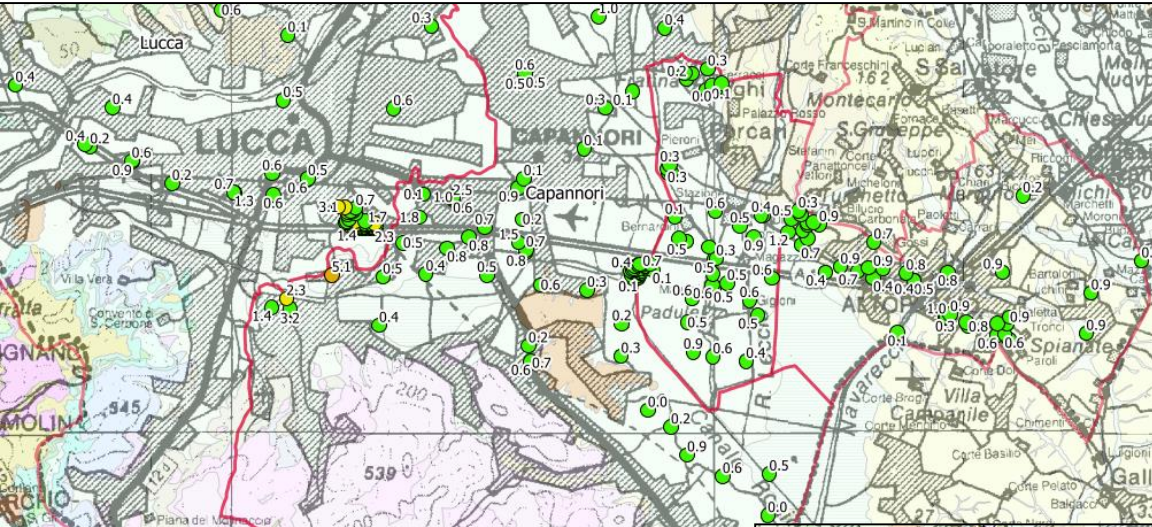
Legenda

Classificazione LPI metodo R&W

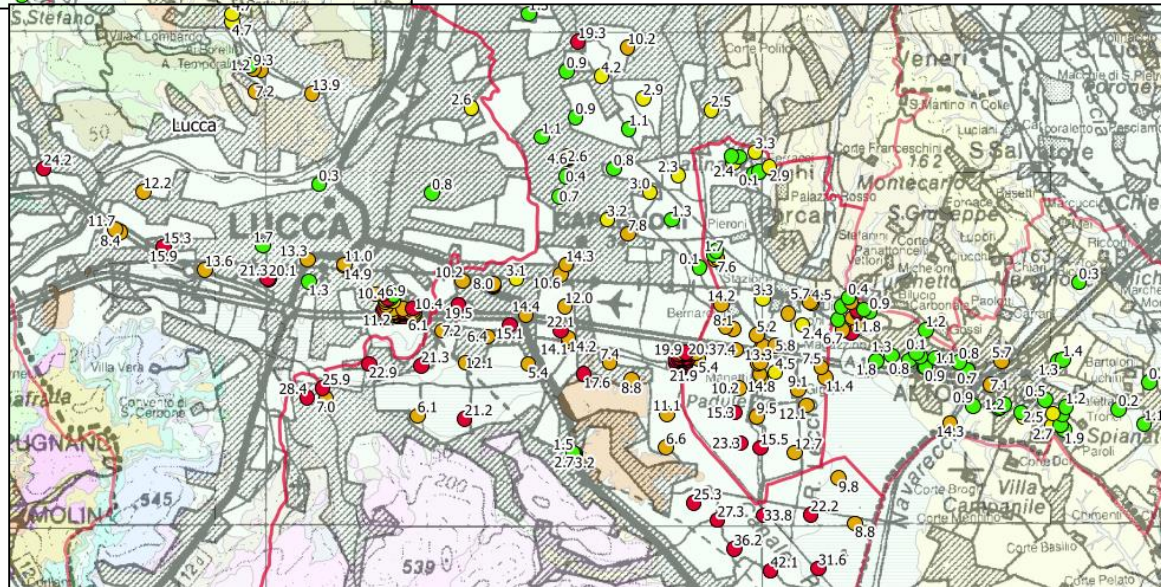
- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15
- Sub progetto LUCCA



Map of liquefaction risk (Lucca plan)



LPI evaluation – Boulanger & Idriss (2014)



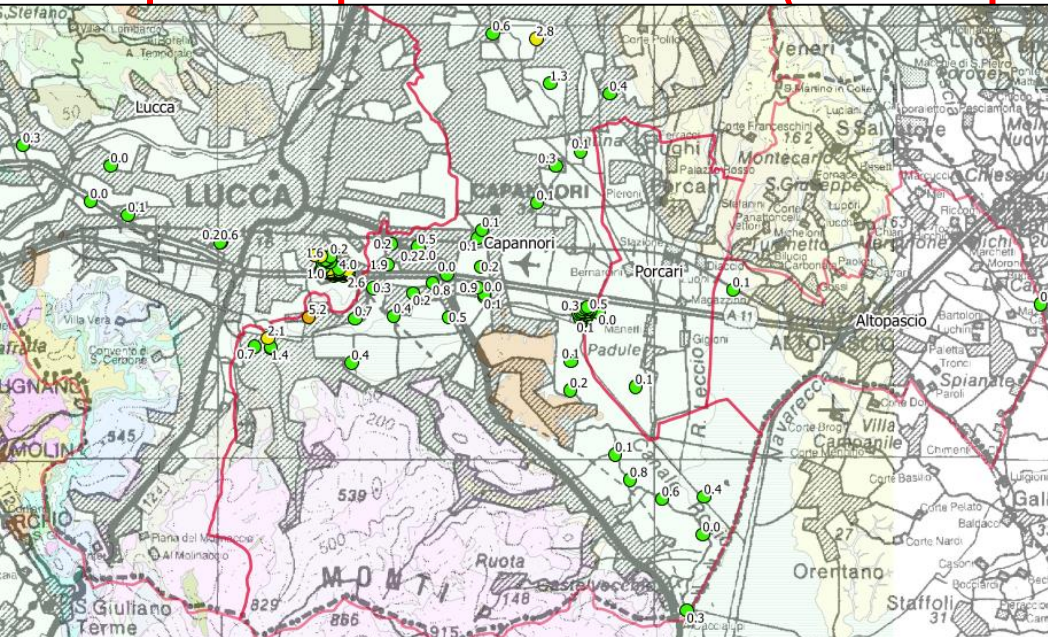
Legenda

Classificazione LPI metodo B&I

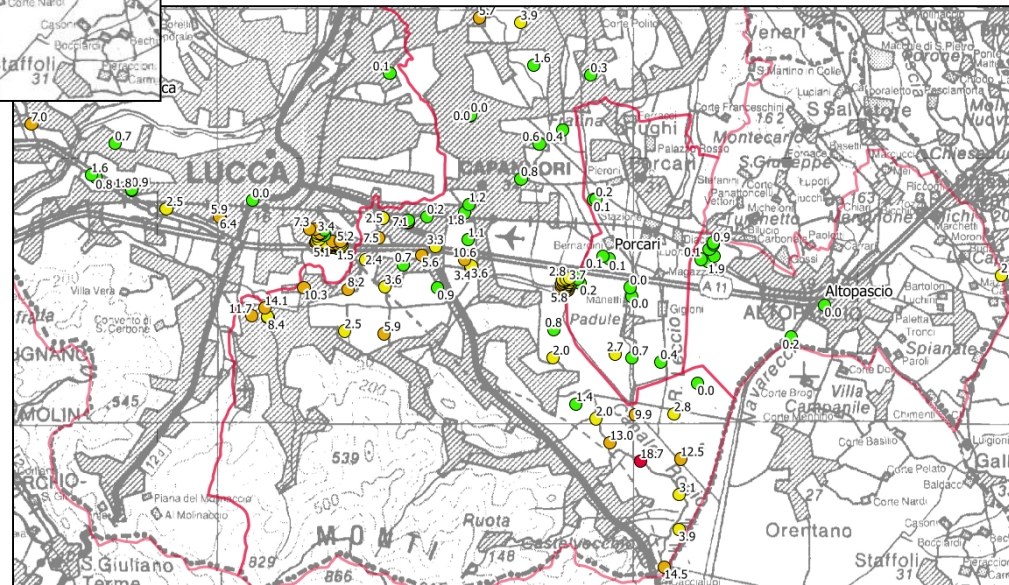
- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15
- Sub progetto LUCCA



Map of liquefaction risk (Lucca plan)



LPI evaluation – Juang et al. (2006)



Legenda

Classificazione LPI metodo J&AL corretto

- classe da 0 a 2
- classe da 2 a 5
- classe da 5 a 15
- classe maggiore di 15
- ▭ Sub progetto LUCCA



Discussion and final remarks

1) The simplified CPT-based procedures selected for these study all gave different results in terms of LPI, overall for soils with intermediate grain-size distribution (clean sands / clays). These differences can be addressed principally to the correction factor proposed for the estimation of the equivalent clean sand cone tip resistance that is generally based on the empirical assessment of the fines content

It's recommended to use multiple methods in order to evaluate the dispersion

2) The influence of correction (CPTe/CPTm) is significant and the liquefaction hazard evaluated at most of the investigated sites changes from low to high or very high

It's recommended to use CPTu-CPTe test to evaluate the LPI

3) The B&I (2014) e R&W (1998) methods provide similar results while Juang et al. (2006) provides less conservative results (but closer to CPTe LPI results and). The application of the correction to the "Juang" methods leads to lower increased LPI values compared to other methods.

It's advisable to use Juang et al. (2006) method for LPI

4) The use of corrections to standard methodology is being studied by the Pisa University (Scientific Resp. Prof. Diego Lo Presti)



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CPT Database of the Tuscany Region



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